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FLIGHT INVESTIGATION OF THE PERFORMANCE AND COOLING
CHARACTERISTICS OF AN NACA C COWLING ON THE XP-42 AIRPLANE

By J. Ford Johnston and Stefan A. Cavallo

Langley Memorial Aeronautical Laboratory
Langley Field, Va.

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MEMORANDUM REPORT

for

Army Air Forces, Materiel Command

FLIGHT INVESTIGATION OF THE PERFORMANCE AND COOLING
CHARACTERISTICS OF AN NACA C COWLING ON THE XP-42 AIRPLANE

By J. Ford Johnston and Stefan A. Cavallo

SUMMARY

Results are presented of high-speed and climb tests of an NACA C cowling on the XP-42 airplane. These tests were made for comparison with tests of NACA type D cowlings on the same airplane.

The top speed corresponding to the engine military power (1000 hp at 14,500 ft) was 336 miles per hour; the addition of Curtiss narrow-chord propeller cuffs increased this speed by 1 mile per hour; and the addition of cuffs and a 24-inch-diameter spinner increased the speed by 3 miles per hour.

Cooling-air-pressure recovery on the front of the engine in climb, at 140 miles per hour indicated airspeed, averaged 58 percent of airplane impact pressure with the spinner and cuffs, 68 percent with cuffs only, and 67 percent without spinner or cuffs. Corresponding pressure recoveries in full-throttle level flight were 69, 74, and 74 percent.

The ground cooling with spinner and cuffs was satisfactory. With cuffs only, spark-plug elbow temperatures exceeded their limit by 29° F after cut-off in the ground run.

Without cuffs or spinner, they exceeded their limit by 65° F, and the oil-in temperature also exceeded its limit.

INTRODUCTION

The NACA has conducted an extensive flight investigation, on the XP-42 airplane, of NACA type D cowlings for radial air-cooled engines. Tests of a long-nose high-inlet-velocity cowling have been reported in reference 1, those of a short-nose high-inlet-velocity cowling in references 2 and 3, and of a short-nose low-inlet-velocity cowling in references 4 and 5. In order to compare these cowlings with the conventional NACA C type now in general use, the flight investigation was extended to include tests of a C cowling, reported herein.

The conditions investigated with the C cowling included:

<u>Test number</u>	<u>Airplane condition</u>
17	C cowling with 2 $\frac{1}{4}$ -inch spinner and narrow-chord propeller cuffs - climb
18	C cowling with 2 $\frac{1}{4}$ -inch spinner and narrow-chord propeller cuffs - high speed
19	C cowling with cuffs only - high speed
20	C cowling with cuffs only - climb
21	C cowling without spinner or cuffs - climb
22	C cowling without spinner or cuffs - high speed

XP-42 AIRPLANE WITH C COWLING

The XP-42 airplane with its P. & W. 1830 engine was described in reference 2. The C cowl external shape (reference 6) was obtained by adding a lip to the D cowling of references 2, 3, 4, and 5. The internal changes consisted of removing the cowl inner liner and the afterbody of the spinner which together formed the diffuser section typical of the D cowling. A dimensioned drawing of the C cowl installation is given in figure 1. Figures 2 and 3 show the airplane with the spinner and cuffs; figures 4 and 5, with cuffs only; and figures 6 and 7, without spinner or cuffs.

The cuffs and spinner were manufactured by the Propeller Division of the Curtiss-Wright Corporation, and were of the standard design for the 10-foot-diameter Curtiss propeller, drawing number 512 cc 1.5.

The modified cowl flaps used in the tests of references 3, 4, and 5 are shown open in figures 2, 3, and 4, and closed in figures 6 and 7.

TEST APPARATUS

The installation of the test equipment was essentially the same as described in reference 2, with the exception that the three pressure survey rakes which had been installed in the annular diffuser section were moved to a position just forward of the front cylinder-valve push rods at the same

120° intervals around the engine. The left rake may be seen inside the cowling in figure 7.

PROCEDURE

The procedure followed in making the high-speed and climb tests is described in references 2 and 4. For each condition, the high speed was determined from two flights of five runs each. The climb tests for each condition consisted of one climb at 155 miles per hour indicated with the mixture control in automatic rich, and one at 140 miles per hour indicated in the full rich setting, in which the altitude compensator is bypassed.

The ground cooling was checked for each condition by a 10-minute run at 1400 rpm with the cowl flaps open and the propeller in the low-pitch position, followed by a 5-minute idling period. Temperatures were recorded during the runs and for approximately 10 minutes after cut-off.

RESULTS

The data obtained during the high-speed level-flight runs and during the climbs are presented in tables 1(a), 1(b), and 2. Time histories of the climbs are shown in figures 8, 9, and 10.

Analyses of the high-speed performance are given in figures 11 and 12. The observed cooling-air pressure distributions in the high-speed and climb conditions are shown in figures 13 and 14, and typical cylinder-head and barrel temperature distributions, in figures 15 through 18.

Time histories of the ground-cooling tests are presented in figures 19, 20, and 21.

Table 3 gives a comparison of the maximum speeds at military power and the average cooling-air-pressure recoveries with all the cowlings tested on the XP-42 airplane.

DISCUSSION

Maximum Speed

The values of maximum speed and power observed during the full-throttle level runs with each arrangement tested are shown on figure 11. The figure also includes the parameters $(\frac{\text{bhp}}{\sigma})^{\frac{1}{3}}$, representative of the effective power, and $52.73 \left(\frac{\eta}{C_{DS}}\right)^{\frac{1}{3}}$, representative of the airplane cleanliness, as explained in references 1 and 2. The product of these two parameters is the speed of the airplane. The installation having the highest value of the latter parameter will evidently have the highest speed at a given power and altitude.

It was shown in reference 4 that the installation of the modified cowl flaps in the closed position caused an increase of form drag, resulting in a decrease of approximately two-thirds of 1 percent in the parameter $52.73 \left(\frac{\eta}{C_{DS}}\right)^{\frac{1}{3}}$. This increase of drag is attributed to air leakage around the modified flaps and would not be present in a well-designed flap installation. Hence, for comparison with the results of previous tests with the original cowl flaps, it is desirable

to increase by two-thirds of 1 percent the values of speed and $52.73 \left(\frac{\eta}{C_{DS}} \right)^{\frac{1}{3}}$ observed in the present tests. This correction of 2 miles per hour, while not shown on figure 11, has been incorporated in the data plotted on figure 12, which presents a comparison of the speeds obtained with the various cowling arrangements tested on the XP-42 airplane. Points corresponding to the official performance figures for similar airplanes with conventional air-cooled (P-36A) and liquid-cooled (P-40C) installations are also shown.

Examination of figure 12 shows that if in each case the engine had delivered its rated military power (1000 hp at 14,500 ft; $\frac{bhp}{\sigma} = 1564$), the speeds would have been as listed in table 3. As explained in reference 1, this figure may be used for comparing the speeds of various installations at the same power and altitude by movement of the test points along lines of constant $\frac{\eta}{C_{DS}}$ to a common value of $\frac{bhp}{\sigma}$. Such a comparison at the rated military power of the engine (1000 hp at 14,500 ft; $\frac{bhp}{\sigma} = 1564$) is presented in table 3 for all the cowling arrangements tested on the XP-42 airplane.

Examination of table 3 shows that the speed with the C cowling was increased 1 mile per hour by the addition of cuffs and 3 miles per hour by the addition of cuffs and a spinner. It appears that an improvement in the external-flow conditions around the cowl nose was obtained by use of the spinner. The pressure recovery data listed in table 3 indicate

that the cuffs were not loaded in the high-speed condition. It is probable that the cuffs served to streamline the propeller shanks and thus to increase the propulsive efficiency.

It should be noted that the fairing material on the nose of the C cowling (see figs. 3, 5, and 7) was subjected to cracking under flight vibration. Although the fairing was smooth before each high-speed test, some cracks appeared during flight. These cracks would cause a premature transition from a laminar to a turbulent boundary layer and a consequent speed loss estimated at not over 1 mile per hour. No correction has been made for this possible source of drag.

Pressures and Temperatures

The average cooling-air pressures on the front of the engine in full-power level flight with each arrangement are listed in table 3. The pressure recovery at high speed averaged approximately $0.74q_c$ for either case without the spinner, and $0.69q_c$ with cuffs and spinner. Engine cooling-air pressure distributions for the three modifications are shown on figure 13 for the high-speed condition. The values plotted are the average over 10 runs for each location of pressure measurement. The pressures noted on the exhaust side of the barrel of cylinder 3 may be expected to be low because points of measurement lay in the wake of a large ignition cable conduit and next to a hole in the baffling.

The pressures as shown in figure 13 are reasonably uniform, but they are, in general, lower than would be expected from an open-nose cowling. The low inlet velocity in either case without the spinner would preclude any but negligible losses from the cowl entrance to the front of the engine. With the spinner, the inlet velocity ratio is estimated at very nearly 0.25, so that the q at inlet would be $0.06q_c$. An assumption that 90 percent of the inlet q is lost in turbulence due to the lack of a diffuser section behind the spinner leads to the conclusion that the impact pressure at the cowl entrance referred to free-stream static pressure must have been $0.69q_c + 0.05q_c = 0.74q_c$, or the same as that without the spinner.

It appears that about $0.26q_c$ becomes unavailable, as far as the internal pressure recovery is concerned, because of the presence of the propeller ahead of the cowling. Reference 7 shows that the pressure recovery of a model of a similar cowling (with air flow) was $0.97q$ without the propeller, $0.57q$ with a model propeller hub, and $0.62q$ with an operating propeller ahead of the cowling.

As listed in table 3, the pressure recovery on the front of the engine in full-power climb at 140 miles per hour was $0.58q_c$ with spinner and cuffs, $0.68q_c$ with cuffs only, and $0.67q_c$ without cuffs or spinner. Recoveries in climb at 155 miles per hour were the same or $0.01q_c$ higher. It is obvious from these data that the cuffs were ineffective

in climb. The loss due to the spinner was 0.10 q_c . This increased loss is associated with the increase in inlet-velocity ratio in climb as compared with the high-speed condition.

Typical pressure distributions in climb are shown on figure 14. It is noted that the highest pressures occurred on the lower left side of the engine (cylinders 8 to 12) as a result of high angle of attack, slipstream rotation, and the right yaw of the airplane associated with the full-power climb condition. This pressure gradient across the face of the engine is characteristic of the open-nose cowling. When the inlet velocity was increased by use of the spinner, the pressure distribution became more nearly uniform, as may be seen in figure 14. The dumping losses previously noted, however, reduced the general pressure level.

Typical distributions of the cylinder-head and barrel temperatures are shown in figure 15 for the high-speed condition, in figures 16 and 17 for two altitude ranges in the full-rich climb condition, and in figure 18 for the automatic-rich climb. These data have not been corrected to the same conditions, but runs made near the same altitude were selected for each comparison. It appears from these figures that variations in mixture strength and other factors from cylinder to cylinder obscure the effect of variations of cooling-air pressure drop around the engine. It is seen

that the temperature distributions are essentially similar in all cases. Comparison of figures 16 and 17 shows that the distribution becomes more uneven as the mixture strength increases with altitude in the full-rich climb.

Ground Cooling

Time histories of representative temperatures observed during the ground cooling runs are shown in figures 19, 20, and 21 for the cowling with spinner and cuffs, with cuffs only, and without spinner or cuffs.

In no case with spinner and cuffs did any of the temperatures become critical when corrected to Army standards. However, the oil-in temperature did come within 1° of its limit of 185° F.

In the test with cuffs only, corrected head and barrel temperatures stayed below their Army limits of 500° and 335° F, respectively, but were slightly higher than the spinner-and-cuff condition. The rear spark-plug elbow of cylinder number 7, which was the hottest elbow measured throughout the ground run, ran 29° over its Army limit of 248° F 7 minutes after cut-off.

Without cuffs or spinner, the temperatures of heads and bases were within their limits, but were noticeably higher than with the other two modifications. Spark-plug-elbow temperatures increased throughout the run until at cut-off they were 19° F over their limit and went to 65° F above the

critical temperature 8 minutes after cut-off. Oil-in temperatures also showed a steady increase, passing their critical, when corrected, $7\frac{1}{2}$ minutes after the start of the run and going to 24° F over in 16 minutes, which was the point of cut-off. The magneto operated within its limit throughout the run.

The large change in air temperatures ahead of and behind cylinder number 1, in each case, shows that the air flow reverses direction after the engine is stopped. The fact that in one case (fig. 21) the maximum front spark-plug elbow exceeded even the maximum rear gasket temperature 7 minutes after cut-off is regarded as further evidence of this forward air flow. Comparison of the air temperatures after cut-off in figures 19 and 20 shows that the spinner had no apparent tendency to trap the air in front of the engine.

The cuffs alone improved the ground cooling, and the addition of the spinner gave further improvement. The effect of the spinner was probably to prevent air leakage forward along the propeller shaft.

Langley Memorial Aeronautical Laboratory,
National Advisory Committee for Aeronautics,
Langley Field, Va., November 24, 1942.

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7. Molloy, Richard C., and Brewster, James H., III: New Research on the Cowling and Cooling of Radial Engines. NACA ARR, May 1942.

Table 11(a) Pressure Data (Sheet 1)

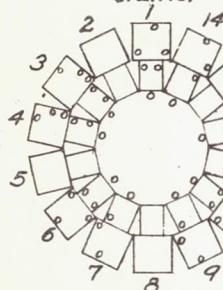
XP-42
AIRPLANE
C. COWL
SPINNER &
CUFFS

TEST NO. - FLT. NO.	18-5					18-6				
RUN NO.	1	2	3	4	5	1	2	3	4	5
TRUE AIR SPEED, MPH	334	336	335	333	335	332	332	332	331	333
QSL, IN. H ₂ O	35.5	34.6	33.3	32.0	31.2	35.3	34.1	33.0	33.3	34.8
ATM. PRESS., IN. HG.	17.53	16.86	16.19	15.56	14.96	17.57	16.88	16.20	16.51	17.22
ATM. TEMP., °F.	34	34	28	23	21	33	28	24	25	33
O ₂ DENSITY RATIO	.616	.592	.576	.559	.540	.618	.600	.581	.590	.606
DENSITY ALT., FT.	15650	16850	17700	18600	19600	15550	16850	174400	17000	16150
BHP	928	905	872	849	821	919	896	868	886	919
RPM	2680					2680				
MANIF. PR., IN. HG.	40.7	39.1	37.8	36.4	35.3	40.5	39.3	37.5	38.4	39.8
	HIGH SPEED					HIGH SPEED				

IND. AIRSPEED, MPH	156	151	153	153	17-4B	1	2	3	4	17-4A
AV. PRESS. ALT.	12.0	11.3	11.5	11.6	17-4B	137	137	138	135	17-4A
AV. FREE AIR, °F	4900	10000	15100	19000	AV. FREE AIR, °F	9.3	9.3	9.4	9.0	AV. FREE AIR, °F
AV. BHP	63	49	33	18	AV. BHP	5.9	4.3	2.8	1.5	AV. BHP
AV. MANIF. PRESS.	860	880	820	710	AV. MANIF. PRESS.	870	900	740	620	AV. MANIF. PRESS.
RPM	40.0	39.0	36.0	30.9	RPM	42.0	42.0	35.0	30.0	RPM
	2560					2560				
	AUTO RICH CLIMB					FULL RICH CLIMB				
	WITH SPINNER & CUFFS					WITH SPINNER & CUFFS				

ENGINE PRESSURE TUBE LOCATIONS

CYL. NO.



	PRESSURE RATIO, P ₁₄ /P ₁									
1-R	.26	.24	.24	.23	.23	.26	.26	.25	.25	.25
3-R	.26	.24	.24	.23	.23	.26	.26	.25	.26	.25
4-R	.25	.24	.23	.22	.22	.25	.25	.24	.25	.24
6-R	.28	.27	.26	.25	.25	.29	.28	.28	.28	.28
7-R	.28	.27	.27	.25	.25	.29	.29	.28	.28	.28
9-R	.29	.27	.27	.25	.26	.29	.29	.28	.28	.28
10-R	.29	.27	.27	.25	.26	.29	.29	.28	.28	.28
12-R	.26	.25	.25	.24	.23	.26	.26	.26	.26	.25
14-R	.26	.24	.24	.23	.23	.26	.26	.25	.25	.25
1-EH	.67	.67	.67	.66	.66	.68	.68	.67	.67	.67
3-EH	.60	.60	.60	.59	.58	.61	.61	.60	.61	.60
4-EH	.71	.70	.69	.68	.68	.70	.69	.69	.70	.70
6-EH	.73	.72	.72	.71	.70	.73	.72	.72	.73	.72
7-EH	.71	.70	.69	.69	.69	.70	.71	.70	.72	.70
9-EH	.73	.73	.72	.72	.71	.73	.74	.73	.74	.73
10-EH	.72	.72	.71	.71	.70	.72	.72	.72	.72	.72
12-EH	.73	.73	.72	.71	.71	.72	.72	.71	.72	.72
14-EH	.74	.73	.73	.72	.71	.72	.72	.72	.72	.72
1-EH	.74	.74	.73	.72	.72	.73	.73	.73	.73	.73
3-EH	.70	.69	.68	.68	.68	.69	.68	.68	.69	.69
4-EH	.73	.73	.71	.71	.71	.72	.71	.71	.72	.72
6-EH	.66	.64	.65	.65	.65	.66	.66	.65	.66	.65
7-EH	.73	.73	.72	.70	.71	.72	.72	.71	.72	.72
9-EH	.68	.67	.66	.66	.66	.68	.67	.67	.67	.67
10-EH	.68	.66	.66	.64	.64	.66	.66	.66	.66	.66
12-EH	.70	.70	.71	.68	.67	.70	.70	.70	.69	.69
14-EH	.72	.71	.71	.69	.68	.72	.70	.71	.70	.70
1-TH	.72	.71	.71	.69	.69	.71	.70	.70	.70	.72
3-TH	.72	.71	.71	.69	.69	.71	.70	.71	.71	.71
4-TH	.70	.70	.68	.67	.67	.69	.69	.69	.70	.68
6-TH	.67	.68	.66	.64	.65	.67	.66	.66	.66	.66
7-TH	.69	.69	.67	.67	.67	.68	.68	.68	.69	.68
9-TH	.70	.71	.71	.70	.69	.70	.70	.70	.70	.70
10-TH	.70	.70	.71	.70	.69	.69	.69	.69	.68	.68
12-TH	.70	.70	.71	.69	.69	.68	.69	.69	.69	.68
14-TH	.65	.65	.65	.65	.63	.66	.65	.64	.64	.67
1-IH	.73	.74	.73	.73	.71	.72	.72	.72	.73	.72
3-IH	.70	.69	.68	.69	.68	.68	.69	.68	.69	.68
10-IH	.75	.76	.75	.74	.73	.74	.73	.74	.74	.74
1-IB	.67	.67	.66	.66	.64	.67	.66	.67	.66	.66
6-IB	.74	.74	.73	.73	.73	.74	.73	.74	.72	.72
10-IB	.72	.73	.72	.72	.70	.72	.72	.72	.73	.71
3-EH2	.63	.63	.63	.62	.61	.62	.62	.62	.61	.63
4-EH2	.70	.70	.69	.68	.68	.70	.69	.69	.70	.70
3-EB2	.54	.55	.55	.54	.54	.55	.55	.55	.54	.54
4-EB2	.60	.60	.60	.60	.60	.61	.61	.60	.63	.62

	PRESSURE RATIO, P ₁₄ /P ₁									
3-TH	.74	.73	.73	.71	.72	.72	.72	.73	.72	.73
3-EH2	.63	.63	.63	.62	.61	.62	.62	.62	.61	.63
3-EB2	.54	.55	.55	.54	.54	.55	.55	.55	.54	.54
3-R	.60	.60	.60	.60	.60	.61	.61	.60	.63	.62

METHOD OF DESIGNATING TUBE LOCATIONS
FOR TYPICAL CYLINDERS

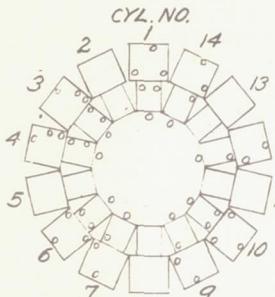
Table 1(a) Pressure Data (Sheet 2)

XP-42
AIRPLANE
C COWL
CUFFS ONLY

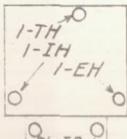
TEST NO.-FLT. NO. RUN NO.	19-1					19-2				
	1	2	3	4	5	1	2	3	4	5
TRUE AIRSPEED, MPH.	332	331	332	330	330	331	331	331	332	334
$\rho_{\text{c}}/ \rho_{\text{in. H}_2\text{O}}$.350	.337	.328	.314	.303	.340	.330	.317	.308	.339
ATM. PRESS., IN. HG.	17.48	16.83	16.16	15.51	14.90	16.89	16.22	15.59	14.94	16.53
ATM. TEMP., °F	33	30	27	21	18	26	23	23	20	27
$\rho_{\text{air}}/\rho_{\text{in. H}_2\text{O}}$.616	.596	.576	.560	.541	.603	.583	.560	.540	.589
DENSITY ALT., FT.	15650	16700	17700	18500	19600	16500	17300	18500	19650	17050
BHP.	9.28	9.00	8.77	8.49	8.16	9.09	8.77	8.53	8.12	9.05
RPM	2680					2580				
MAN. PRESS., IN. HG.	40.5	39.0	37.6	36.3	34.9	39.2	38.0	36.5	35.0	38.6
HIGH SPEED, FULL THROTTLE										

IND. AIRSPEED, MPH.	1	2	3	4	1	2	3	4
$\rho_{\text{in. H}_2\text{O}}$	155	154	153	152	140	139	139	136
AV. PRESS. ALT.	12.0	11.8	11.6	11.5	9.7	9.5	9.5	9.2
AV. FREE AIR, °F	3800	9100	13900	18900	3800	8800	14000	17800
AV. BHP	66	48	34	21	69	48	31	21
AV. MAN. PRESS. RPM	870	900	840	750	930	930	780	660
← 2580 →				← 2570 →				
AUTO RICH CLIMB				FULL RICH CLIMB				
WITH CUFFS				WITHOUT SPINNER				

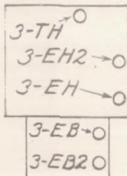
ENGINE PRESSURE
TUBE LOCATIONS



METHOD OF DESIGNATING TUBE LOCATIONS
FOR TYPICAL CYLINDERS



Cyl. no. 1



Cyl. no. 3

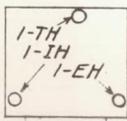
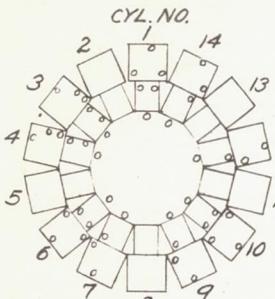
PRESSURE RATIO, $\frac{P_{\text{out}}}{P_{\text{in. H}_2\text{O}}}$										
1-R	.27	.26	.26	.25	.26	.27	.28	.26	.27	.27
3-R	.27	.26	.26	.25	.26	.27	.28	.26	.26	.26
4-R	.25	.26	.26	.24	.25	.27	.27	.26	.26	.26
6-R	.29	.28	.29	.28	.28	.29	.29	.28	.28	.29
7-R	.30	.29	.30	.28	.28	.30	.29	.28	.28	.28
9-R	.30	.29	.30	.28	.29	.31	.31	.30	.30	.29
10-R	.30	.29	.30	.28	.29	.31	.30	.29	.30	.29
12-R	.27	.27	.27	.26	.26	.28	.28	.27	.27	.28
14-R	.27	.26	.26	.25	.26	.27	.28	.26	.26	.27
1-EB	.73	.72	.73	.71	.72	.72	.71	.72	.72	.74
3-EB	.63	.63	.62	.63	.62	.63	.62	.62	.64	.64
4-EB	.73	.73	.73	.73	.72	.72	.73	.72	.74	.74
6-EB	.78	.78	.78	.78	.77	.77	.78	.77	.78	.78
7-EB	.76	.77	.75	.75	.77	.75	.75	.76	.76	.76
9-EB	.79	.79	.80	.78	.80	.78	.78	.79	.78	.78
10-EB	.78	.77	.78	.77	.78	.76	.78	.77	.78	.76
12-EB	.79	.77	.78	.76	.78	.77	.80	.77	.78	.78
14-EB	.79	.80	.79	.78	.78	.79	.80	.78	.79	.79
1-EH	.81	.80	.80	.79	.80	.81	.80	.80	.80	.80
3-EH	.70	.70	.70	.69	.70	.70	.70	.69	.71	.71
4-EH	.74	.75	.74	.75	.74	.74	.74	.73	.73	.76
6-EH	.70	.70	.71	.71	.71	.72	.70	.70	.71	.71
7-EH	.79	.78	.78	.78	.79	.78	.79	.78	.78	.78
9-EH	.76	.75	.76	.76	.76	.77	.75	.75	.75	.75
10-EH	.76	.76	.76	.76	.76	.77	.75	.76	.75	.75
12-EH	.77	.77	.76	.76	.76	.77	.78	.76	.77	.76
14-EH	.79	.79	.78	.77	.79	.80	.79	.78	.78	.78
1-TH	.79	.79	.79	.77	.79	.79	.79	.78	.79	.79
3-TH	.75	.75	.76	.75	.76	.76	.74	.74	.76	.76
4-TH	.75	.75	.75	.74	.75	.76	.75	.74	.75	.75
6-TH	.74	.74	.74	.74	.75	.75	.74	.72	.75	.75
7-TH	.76	.75	.76	.75	.76	.76	.75	.75	.75	.75
9-TH	.80	.79	.79	.79	.80	.79	.80	.78	.79	.78
10-TH	.80	.79	.79	.79	.78	.80	.78	.78	.80	.78
12-TH	.78	.77	.77	.76	.77	.77	.79	.77	.78	.76
14-TH	.73	.73	.73	.73	.73	.74	.73	.73	.72	.72
1-IH	.80	.79	.80	.80	.80	.79	.79	.79	.79	.79
6-IH	.77	.77	.76	.77	.77	.76	.75	.74	.76	.76
10-IH	.79	.79	.80	.78	.80	.79	.81	.78	.79	.77
1-EB	.73	.72	.73	.72	.73	.72	.72	.72	.73	.73
6-EB	.79	.78	.78	.78	.79	.78	.79	.78	.78	.78
10-EB	.77	.77	.77	.78	.76	.76	.79	.77	.77	.75
3-EH2	.63	.63	.64	.63	.63	.62	.63	.63	.64	.64
4-EH2	.71	.72	.70	.71	.72	.70	.71	.69	.72	.72
3-EB2	.58	.58	.58	.58	.59	.58	.59	.58	.58	.58
4-EB2	.60	.61	.60	.61	.60	.59	.59	.60	.59	.61

-.34	-.34	-.35	-.34	-.34	-.42	-.42	-.40	-.40
-.31	-.33	-.32	-.32	-.32	-.35	-.37	-.40	-.36
-.35	-.38	-.37	-.36	-.36	-.40	-.44	-.43	-.40
-.19	-.21	-.20	-.21	-.21	-.23	-.24	-.29	-.22
-.18	-.19	-.20	-.21	-.21	-.23	-.24	-.29	-.22
-.18	-.21	-.20	-.19	-.19	-.23	-.24	-.29	-.27
-.21	-.21	-.22	-.21	-.21	-.26	-.27	-.28	-.28
-.30	-.33	-.32	-.32	-.32	-.38	-.40	-.38	-.38
-.32	-.34	-.34	-.34	-.34	-.40	-.42	-.38	-.38
-.54	.58	.57	.57	.58	.53	.50	.52	.52
.42	.41	.40	.45	.45	.38	.38	.38	.44
.66	.61	.63	.67	.67	.63	.63	.69	.69
.80	.78	.78	.76	.76	.74	.74	.77	.77
.75	.76	.72	.72	.72	.74	.73	.70	.70
.83	.80	.84	.82	.82	.84	.82	.81	.81
.83	.83	.82	.84	.84	.84	.82	.82	.84
.77	.79	.78	.76	.76	.79	.76	.76	.72
.72	.73	.71	.72	.72	.76	.66	.65	.67
.68	.69	.67	.67	.67	.66	.65	.65	.67
.50	.50	.50	.53	.53	.50	.49	.50	.50
.61	.60	.61	.66	.66	.64	.64	.61	.65
.66	.64	.67	.64	.64	.68	.69	.61	.67
.79	.79	.78	.84	.84	.82	.82	.78	.79
.74	.75	.74	.75	.75	.75	.75	.71	.74
.78	.76	.78	.77	.77	.81	.78	.73	.78
.88	.87	.82	.85	.88	.87	.87	.87	.87
.73	.74	.72	.73	.73	.76	.72	.73	.71
.67	.66	.68	.67	.68	.64	.62	.62	.66
.62	.61	.60	.60	.60	.58	.61	.60	.62
.65	.65	.65	.65	.65	.65	.66	.65	.65
.69	.66	.70	.69	.67	.67	.68	.62	.66
.76	.73	.72	.75	.75	.77	.74	.71	.74
.85	.83	.82	.82	.82	.85	.80	.80	.80
.81	.80	.82	.82	.82	.84	.80	.76	.78
.88	.87	.82	.83	.83	.89	.87	.90	.87
.62	.63	.63	.64	.64	.61	.58	.55	.56
.72	.72	.71	.69	.69	.64	.65	.63	.65
.78	.78	.75	.73	.73	.79	.74	.72	.69
.91	.90	.92	.89	.89	.95	.94	.91	.90
.54	.57	.56	.57	.57	.52	.52	.52	.53
.80	.80	.80	.81	.81	.84	.80	.77	.79
.84	.83	.82	.83	.83	.88	.85	.86	.87
.37	.38	.39	.41	.41	.37	.34	.34	.40
.57	.58	.60	.58	.64	.61	.59	.59	.59
.31	.31	.32	.34	.26	.26	.26	.26	.29
.50	.46	.47	.51	.47	.52	.46	.46	.52

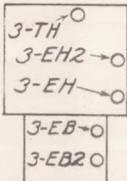
Table 1(a) Pressure Data (Sheet 3)

XP-42
AIRPLANE
C COWL
NO CUFFS OR
SPINNER

TEST NO. - FLT. NO.	22-1					22-2				
RUN NO.	1	2	3	4	5	1	2	3	4	5
TRUE AIRSPEED, MPH.	331	331	331	330	330	329	329	330	330	327
ρ_e IN. H ₂ O	34.6	33.7	32.3	31.0	30.3	33.9	32.8	31.9	30.8	29.2
ATM. PRESS., IN. HG.	17.23	16.54	15.90	15.27	14.66	17.16	16.47	15.84	15.19	14.60
ATM. TEMP., °F	28	23	23	19	13	28	26	23	21	19
σ DENSITY RATIO	.616	.594	.571	.553	.538	.610	.588	.569	.548	.529
DENSITY ALT., FT.	15650	16750	17950	18900	19700	15950	17050	18050	19150	20200
BHP	928	900	877	840	816	919	891	863	830	793
RPM						2680				
MANIF. PR., IN. HG.	39.9	38.2	36.8	35.3	34.2	39.7	38.1	36.6	35.3	33.9

ENGINE PRESSURE
TUBE LOCATIONS

Cyl. no. 1



Cyl. no. 3

METHOD OF DESIGNATING TUBE LOCATIONS
FOR TYPICAL CYLINDERS

	PRESSURE RATIO, P ₁ /P ₀									
	.22	.22	.23	.22	.22	.25	.26	.24	.23	.25
1-R	.22	.22	.23	.22	.22	.24	.26	.24	.23	.25
3-R	.22	.22	.23	.22	.22	.24	.26	.24	.23	.25
4-R	.20	.20	.21	.21	.20	.23	.25	.22	.23	.24
6-R	.25	.26	.26	.26	.26	.29	.30	.28	.27	.29
7-R	.25	.26	.26	.26	.25	.29	.30	.28	.27	.29
9-R	.26	.26	.27	.26	.26	.29	.31	.28	.28	.30
10-R	.26	.26	.27	.26	.26	.29	.30	.28	.27	.30
12-R	.23	.23	.24	.23	.23	.26	.27	.25	.24	.26
14-R	.22	.22	.23	.22	.22	.25	.26	.24	.24	.25
1-EB	.72	.72	.72	.72	.72	.73	.73	.72	.73	.73
3-EB	.61	.62	.62	.61	.62	.62	.63	.61	.63	.63
4-EB	.71	.73	.74	.72	.73	.73	.74	.72	.74	.73
6-EB	.76	.76	.78	.77	.77	.77	.79	.77	.78	.79
7-EB	.75	.75	.76	.76	.76	.76	.78	.76	.74	.78
9-EB	.78	.79	.79	.79	.78	.79	.81	.80	.79	.81
10-EB	.77	.76	.77	.77	.77	.77	.79	.78	.78	.78
12-EB	.78	.79	.79	.78	.78	.79	.80	.79	.79	.80
14-EB	.80	.79	.80	.78	.78	.80	.80	.80	.80	.80
1-EH	.80	.80	.81	.80	.79	.80	.82	.80	.81	.80
3-EH	.68	.69	.69	.69	.70	.69	.70	.70	.70	.69
4-EH	.73	.74	.75	.73	.73	.74	.75	.73	.74	.74
6-EH	.71	.72	.72	.72	.72	.73	.72	.72	.73	.73
7-EH	.77	.78	.78	.76	.78	.78	.80	.79	.79	.79
9-EH	.75	.76	.75	.74	.75	.76	.78	.76	.77	.77
10-EH	.76	.75	.76	.75	.75	.76	.78	.76	.76	.78
12-EH	.78	.77	.78	.77	.77	.79	.79	.77	.78	.79
14-EH	.78	.79	.80	.79	.78	.80	.81	.80	.80	.80
1-TH	.78	.80	.80	.79	.79	.81	.82	.81	.81	.81
3-TH	.74	.75	.76	.74	.75	.75	.76	.74	.75	.76
4-TH	.75	.76	.76	.75	.75	.75	.78	.74	.76	.77
6-TH	.75	.75	.76	.75	.75	.76	.77	.76	.76	.77
7-TH	.76	.76	.76	.75	.76	.76	.78	.76	.76	.77
9-TH	.79	.79	.79	.79	.80	.80	.80	.79	.81	.81
10-TH	.82	.78	.80	.79	.78	.80	.80	.78	.80	.82
12-TH	.78	.78	.79	.78	.78	.80	.80	.78	.80	.80
14-TH	.73	.74	.75	.74	.74	.75	.76	.76	.75	.75
1-IH	.79	.79	.80	.79	.78	.80	.80	.80	.80	.80
6-IH	.76	.75	.76	.77	.76	.76	.77	.77	.76	.78
10-IH	.78	.78	.78	.79	.78	.80	.80	.78	.80	.81
1-IB	.71	.72	.73	.72	.72	.74	.72	.73	.72	.72
6-IB	.78	.75	.79	.78	.76	.78	.80	.78	.78	.79
10-IB	.76	.76	.76	.76	.76	.77	.78	.76	.77	.79
3-EH2	.61	.62	.62	.62	.62	.62	.63	.62	.64	.62
4-EH2	.71	.72	.72	.72	—	.71	.73	.72	.71	.72
3-EB2	.56	.56	.57	.56	.56	.57	.58	.57	.58	.59
4-EB2	.57	.59	.61	.59	.60	.60	.60	.61	.61	.60

IND. AIRSPEED, MPH.	21-1A					21-1B						
AV. PRESS. ALT.	1	2	3	4	1	2	3	4	1	2	3	4
4200	155	153	154	153	139	138	136	135	11.9	11.6	11.7	11.5
5200	4200	8900	14200	17800	3900	9700	13800	17700	9.5	9.4	9.2	9.0
5300	52	49	37	23	53	51	36	20	4.0	4.0	4.0	4.0
5350	930	930	840	760	1000	940	790	680	4.5	4.5	4.5	4.5
5400	39.8	40.0	36.1	31.8	43.0	42.0	36.0	30.8	4.0	4.0	4.0	4.0
					25.60				2.540			

AUTO. RICH CLIMB
NO SPINNER OR CUFFS

FULL RICH CLIMB

Table 1(b) Pressure Data (Sheet 1)

XP-42 AIRPLANE C COWL SPINNER & CUFFS	TEST NO.-FLT NO. RUN NO.	18-5					18-6					IND AIRSPEED, MPH	17-4B				17-4A			
		1	2	3	4	5	1	2	3	4	5		1	2	3	4	1	2	3	4
TRUE AIRSPEED	334	336	335	333	335	332	332	332	331	333	334	156	151	153	153	137	137	138	135	
Q _c ; INCHES H ₂ O	355	34.6	33.3	32.0	31.2	353	34.1	33.0	33.3	34.8	12.0	11.3	11.5	11.6	9.3	9.3	9.4	9.0		
ATM. PRESS. IN. HG	17.53	16.86	16.19	15.56	14.96	17.57	16.88	16.20	16.51	17.22	4900	10000	15100	19000	5200	9900	15100	19000		
ATM TEMP. °F	34	34	28	23	21	33	28	24	25	33	63	49	33	18	59	43	28	15		
G, DENSITY RATIO	.616	.592	.576	.559	.540	.618	.600	.581	.590	.606	860	880	820	710	870	900	740	620		
DENSITY ALT., FT.	15650	14850	17700	19600	19000	15550	16450	17400	17000	16150	40.0	39.0	36.0	30.9	42.0	42.0	35.0	30.0		
BHP	928	905	872	849	821	919	896	868	886	919	2560					2540				
RPM						2680					AUTO RICH CLIMB					FULL RICH CLIMB				
MANIF. PR., IN HG	40.7	39.1	37.8	36.4	35.3	40.5	39.3	37.5	38.4	39.8	SPINNER AND CUFFS									
						HIGH SPEED														
		PRESSURE RATIO P/q _c																		
		A-TP1	1	2	3	4	5	1	2	3	4	5	1	2	3	4	1	2	3	4
		A-TS3	1	2	3	4	5	1	2	3	4	5	1	2	3	4	1	2	3	4
		A-TS1	1	2	3	4	5	1	2	3	4	5	1	2	3	4	1	2	3	4
		A-TP1	1	2	3	4	5	1	2	3	4	5	1	2	3	4	1	2	3	4
		A-RP1	1	2	3	4	5	1	2	3	4	5	1	2	3	4	1	2	3	4
		A-RP1	1	2	3	4	5	1	2	3	4	5	1	2	3	4	1	2	3	4
		A-RS1	1	2	3	4	5	1	2	3	4	5	1	2	3	4	1	2	3	4
		A-LP1	1	2	3	4	5	1	2	3	4	5	1	2	3	4	1	2	3	4
		A-LP1	1	2	3	4	5	1	2	3	4	5	1	2	3	4	1	2	3	4
		A-LS1	1	2	3	4	5	1	2	3	4	5	1	2	3	4	1	2	3	4
		O-FP1	1	2	3	4	5	1	2	3	4	5	1	2	3	4	1	2	3	4
		O-FS1	1	2	3	4	5	1	2	3	4	5	1	2	3	4	1	2	3	4
		O-FP2	1	2	3	4	5	1	2	3	4	5	1	2	3	4	1	2	3	4
		O-FP3	1	2	3	4	5	1	2	3	4	5	1	2	3	4	1	2	3	4
		O-FS2	1	2	3	4	5	1	2	3	4	5	1	2	3	4	1	2	3	4
		O-FS3	1	2	3	4	5	1	2	3	4	5	1	2	3	4	1	2	3	4
		O-RP1	1	2	3	4	5	1	2	3	4	5	1	2	3	4	1	2	3	4
		O-RP2	1	2	3	4	5	1	2	3	4	5	1	2	3	4	1	2	3	4
		O-RP3	1	2	3	4	5	1	2	3	4	5	1	2	3	4	1	2	3	4
		O-RM	1	2	3	4	5	1	2	3	4	5	1	2	3	4	1	2	3	4
		O-FS3	1	2	3	4	5	1	2	3	4	5	1	2	3	4	1	2	3	4
		O-SP1	1	2	3	4	5	1	2	3	4	5	1	2	3	4	1	2	3	4
		C-P1	1	2	3	4	5	1	2	3	4	5	1	2	3	4	1	2	3	4
		C-P2	1	2	3	4	5	1	2	3	4	5	1	2	3	4	1	2	3	4
		C-P3	1	2	3	4	5	1	2	3	4	5	1	2	3	4	1	2	3	4
		C-P4	1	2	3	4	5	1	2	3	4	5	1	2	3	4	1	2	3	4
		C-P5	1	2	3	4	5	1	2	3	4	5	1	2	3	4	1	2	3	4
		C-S1	1	2	3	4	5	1	2	3	4	5	1	2	3	4	1	2	3	4
		C-S2	1	2	3	4	5	1	2	3	4	5	1	2	3	4	1	2	3	4
		C-S3	1	2	3	4	5	1	2	3	4	5	1	2	3	4	1	2	3	4
		C-S4	1	2	3	4	5	1	2	3	4	5	1	2	3	4	1	2	3	4
		C-S5	1	2	3	4	5	1	2	3	4	5	1	2	3	4	1	2	3	4
		C-TH	1	2	3	4	5	1	2	3	4	5	1	2	3	4	1	2	3	4
		IMPACT PRESS. IN CARB.	1	2	3	4	5	1	2	3	4	5	1	2	3	4	1	2	3	4

NATIONAL ADVISORY
COMMITTEE FOR AERONAUTICS

TABLE 11(b) PRESSURE DATA (SHEET 3)

TEST NO. - FLT. NO.	19-1					19-2					20-1					20-2				
	TRUE AIRSPEED	333	334	4	5	331	332	3	4	331	332	3	4	334	335	4	5	IND. AIRSPEED, MPH		
TRUE AIRSPEED	333	334	332	330	331	332	330	3	4	331	332	3	4	334	335	4	5	153		
C. COWL CUFFS ONLY	355.0	355.1	354.8	354.7	354.9	354.8	354.7	3	4	354.8	354.7	3	4	354.9	355.0	4	5	139		
ATM. PRESS. IN. Hg	16.16	16.16	16.16	16.16	16.16	16.16	16.16	3	4	16.22	16.22	3	4	16.53	16.53	4	5	136		
ATM. TEMP. °F	17.48	17.48	17.48	17.48	17.48	17.48	17.48	3	4	14.90	14.90	3	4	14.94	14.94	4	5	9.7		
ATM. DENSITY RATIO	1.0	1.0	1.0	1.0	1.0	1.0	1.0	3	4	1.551	1.551	3	4	1.551	1.551	4	5	17800		
DENSITY ALT., FT	15650	15650	15650	15650	15650	15650	15650	3	4	1616	1616	3	4	1622	1622	4	5	14000		
DBH	9.28	9.28	9.28	9.28	9.28	9.28	9.28	3	4	1.8	1.8	3	4	1.8	1.8	4	5	17800		
MANIF. PR. IN HG	40.5	40.5	40.5	40.5	40.5	40.5	40.5	3	4	5.96	5.96	3	4	5.96	5.96	4	5	18000		
MANIF. PR. IN HG	39.0	39.0	39.0	39.0	39.0	39.0	39.0	3	4	5.76	5.76	3	4	5.76	5.76	4	5	18500		
HIGH SPEED								3	4	5.60	5.60	3	4	5.60	5.60	4	5	19050		
HIGH SPEED								3	4	5.41	5.41	3	4	5.41	5.41	4	5	19500		
HIGH SPEED								3	4	5.20	5.20	3	4	5.20	5.20	4	5	20050		
HIGH SPEED								3	4	4.99	4.99	3	4	4.99	4.99	4	5	20500		
HIGH SPEED								3	4	4.78	4.78	3	4	4.78	4.78	4	5	21050		
HIGH SPEED								3	4	4.57	4.57	3	4	4.57	4.57	4	5	21600		
HIGH SPEED								3	4	4.36	4.36	3	4	4.36	4.36	4	5	22150		
HIGH SPEED								3	4	4.15	4.15	3	4	4.15	4.15	4	5	22700		
HIGH SPEED								3	4	3.94	3.94	3	4	3.94	3.94	4	5	23250		
HIGH SPEED								3	4	3.73	3.73	3	4	3.73	3.73	4	5	23800		
HIGH SPEED								3	4	3.52	3.52	3	4	3.52	3.52	4	5	24350		
HIGH SPEED								3	4	3.31	3.31	3	4	3.31	3.31	4	5	24900		
HIGH SPEED								3	4	3.10	3.10	3	4	3.10	3.10	4	5	25450		
HIGH SPEED								3	4	2.89	2.89	3	4	2.89	2.89	4	5	26000		
HIGH SPEED								3	4	2.68	2.68	3	4	2.68	2.68	4	5	26550		
HIGH SPEED								3	4	2.47	2.47	3	4	2.47	2.47	4	5	27100		
HIGH SPEED								3	4	2.26	2.26	3	4	2.26	2.26	4	5	27650		
HIGH SPEED								3	4	2.05	2.05	3	4	2.05	2.05	4	5	28200		
HIGH SPEED								3	4	1.84	1.84	3	4	1.84	1.84	4	5	28750		
HIGH SPEED								3	4	1.63	1.63	3	4	1.63	1.63	4	5	29300		
HIGH SPEED								3	4	1.42	1.42	3	4	1.42	1.42	4	5	29850		
HIGH SPEED								3	4	1.21	1.21	3	4	1.21	1.21	4	5	30400		
HIGH SPEED								3	4	0.99	0.99	3	4	0.99	0.99	4	5	30950		
HIGH SPEED								3	4	0.78	0.78	3	4	0.78	0.78	4	5	31500		
HIGH SPEED								3	4	0.57	0.57	3	4	0.57	0.57	4	5	32050		
HIGH SPEED								3	4	0.36	0.36	3	4	0.36	0.36	4	5	32600		
HIGH SPEED								3	4	0.15	0.15	3	4	0.15	0.15	4	5	33150		
HIGH SPEED								3	4	0.00	0.00	3	4	0.00	0.00	4	5	33700		
HIGH SPEED								3	4	0.00	0.00	3	4	0.00	0.00	4	5	34250		
HIGH SPEED								3	4	0.00	0.00	3	4	0.00	0.00	4	5	34800		
HIGH SPEED								3	4	0.00	0.00	3	4	0.00	0.00	4	5	35350		
HIGH SPEED								3	4	0.00	0.00	3	4	0.00	0.00	4	5	35900		
HIGH SPEED								3	4	0.00	0.00	3	4	0.00	0.00	4	5	36450		
HIGH SPEED								3	4	0.00	0.00	3	4	0.00	0.00	4	5	37000		
HIGH SPEED								3	4	0.00	0.00	3	4	0.00	0.00	4	5	37550		
HIGH SPEED								3	4	0.00	0.00	3	4	0.00	0.00	4	5	38100		
HIGH SPEED								3	4	0.00	0.00	3	4	0.00	0.00	4	5	38650		
HIGH SPEED								3	4	0.00	0.00	3	4	0.00	0.00	4	5	39200		
HIGH SPEED								3	4	0.00	0.00	3	4	0.00	0.00	4	5	39750		
HIGH SPEED								3	4	0.00	0.00	3	4	0.00	0.00	4	5	40300		
HIGH SPEED								3	4	0.00	0.00	3	4	0.00	0.00	4	5	40850		
HIGH SPEED								3	4	0.00	0.00	3	4	0.00	0.00	4	5	41400		
HIGH SPEED								3	4	0.00	0.00	3	4	0.00	0.00	4	5	41950		
HIGH SPEED								3	4	0.00	0.00	3	4	0.00	0.00	4	5	42500		
HIGH SPEED								3	4	0.00	0.00	3	4	0.00	0.00	4	5	43050		
HIGH SPEED								3	4	0.00	0.00	3	4	0.00	0.00	4	5	43600		
HIGH SPEED								3	4	0.00	0.00	3	4	0.00	0.00	4	5	44150		
HIGH SPEED								3	4	0.00	0.00	3	4	0.00	0.00	4	5	44700		
HIGH SPEED								3	4	0.00	0.00	3	4	0.00	0.00	4	5	45250		
HIGH SPEED								3	4	0.00	0.00	3	4	0.00	0.00	4	5	45800		
HIGH SPEED								3	4	0.00	0.00	3	4	0.00	0.00	4	5	46350		
HIGH SPEED								3	4	0.00	0.00	3	4	0.00	0.00	4	5	46900		
HIGH SPEED								3	4	0.00	0.00	3	4	0.00	0.00	4	5	47450		
HIGH SPEED								3	4	0.00	0.00	3	4	0.00	0.00	4	5	47900		
HIGH SPEED								3	4	0.00	0.00	3	4	0.00	0.00	4	5	48450		
HIGH SPEED								3	4	0.00	0.00	3	4	0.00	0.00	4	5	48900		
HIGH SPEED								3	4	0.00	0.00	3	4	0.00	0.00	4	5	49450		
HIGH SPEED								3	4	0.00	0.00	3	4	0.00	0.00	4	5	49900		
HIGH SPEED								3	4	0.00	0.00	3	4	0.00	0.00	4	5	50450		
HIGH SPEED								3	4	0.00	0.00	3	4	0.00	0.00	4	5	50900		
HIGH SPEED								3	4	0.00	0.00	3	4	0.00	0.00	4	5	51450		
HIGH SPEED								3	4	0.00	0.00	3	4	0.00	0.00	4	5	51900		
HIGH SPEED								3	4	0.00	0.00	3	4	0.00	0.00	4	5	52450		
HIGH SPEED								3	4	0.00	0.00	3	4	0.00	0.00	4	5	52900		
HIGH SPEED								3	4	0.00	0.00	3	4	0.00	0.00	4	5	53450		
HIGH SPEED								3	4	0.00	0.00	3	4	0.00	0.00	4	5	53900		
HIGH SPEED								3	4	0.00	0.00	3	4	0.00	0.00	4	5	54450		
HIGH SPEED								3	4	0.00	0.00	3	4	0.00	0.00	4	5	54900		
HIGH SPEED								3	4	0.00	0.00	3	4	0.00	0.00	4	5	55450		
HIGH SPEED								3	4	0.00	0.00	3	4	0.00	0.00	4	5	55900		
HIGH SPEED								3	4	0.00	0.00	3	4	0.00	0.00	4	5	56450		
HIGH SPEED								3	4	0.00	0.00	3	4	0.00	0.00	4	5	56900		
HIGH SPEED								3	4	0.00	0.00	3	4	0.00	0.00	4	5	57450		
HIGH SPEED								3	4	0.00	0.00	3	4	0.00	0.00	4	5	57900		
HIGH SPEED								3	4	0.00	0.00	3	4	0.00	0.00	4	5	58450		
HIGH SPEED								3	4	0.00	0.00	3	4	0.00	0.00	4	5	58900		
HIGH SPEED								3	4	0.00	0.00	3	4	0.00	0.00	4	5	59450		
HIGH SPEED								3	4	0.00	0.00	3	4	0.00	0.00	4	5	59900		
HIGH SPEED								3	4	0.00	0.00	3	4	0.00	0.00	4	5	60450		
HIGH SPEED</td																				

TABLE 1(b) PRESSURE DATA (SHEET 3)

COMMITTEE FOR AERONAUTICS

TABLE 2

TEMPERATURE DATA (SHEET 1)

TEST NO-FLIGHT NO. RUN NO.	18-5					18-6					17-4B					17-4A				
	1	2	3	4	5	1	2	3	4	5	1	2	3	4	1	2	3	4		
TRUE AIRSPEED, M.P.H.	334	336	335	333	335	332	332	332	331	333	IND. AIRSPEED	154	152	154	154	140	138	137	135	
Q _c IN H ₂ O	35.5	34.6	33.3	32.0	31.2	35.3	34.1	33.0	33.3	34.8	Q _c IN H ₂ O	11.7	11.4	11.7	11.7	9.6	9.4	9.3	9.0	
ATM. PRESS. IN. HG.	17.53	16.86	16.19	15.56	14.96	17.57	16.88	16.20	16.51	17.22	AVE. PRESS. ALT.	5000	10700	15400	18800	6600	10200	16000	19100	
ATM. TEMP. °F	34	34	28	23	21	33	28	24	25	33	AVE. FREE AIR, °F	63	47	32	19	55	43	26	15	
ρ DENSITY RATIO	616	592	576	559	540	618	600	581	590	606	AVE. B.H.P.	860	900	810	710	928	890	718	639	
DENSITY ALT., FT.	15650	16850	17700	18600	19600	15550	16450	17400	17000	16150	AVE. MANIF. PRESS.	400	39.1	356	31.0	43.2	41.5	33.9	30.0	
B.H.P.	928	905	872	849	821	919	896	868	886	919	R. P. M.	2560	2540	2540	2540					
R.P.M.						2620					AUTO RICH CLIMB									
MAN. PRESS. IN. HG						40.7	39.1	37.8	36.4	35.3	HIGH SPEED	40.5	39.3	37.5	38.4	39.8				
CYL NO. PT. OF MEASUREMENT						TEMP. °F					TEMP. °F									
1 - REAR 3P. PL. GASKET	391	389	391	399	422	392	389	398	398	398	328	393	412	424	390	386	346	335		
2	382	382	387	394	418	387	387	396	396	396	324	384	397	402	375	370	337	321		
3	397	394	399	403	430	396	394	403	401	401	335	395	408	419	390	384	350	337		
4	399	394	399	403	432	401	396	403	398	396	321	399	399	412						
5						394	392	399	403	425	335	386	399	408	377	370	353	353		
6						448	452	455	461	487	375	443	466	470	426	424	417	404		
7						416	419	423	426	451	355	408	430	437	406	404	393	381		
8						429	430	437	439	462	359	417	442	446	406	404	399	386		
9						442	442	448	451	480	361	424	450	457	410	408	399	390		
10						414	416	421	426	448	350	406	428	433	395	393	381	368		
11						307	306	309	312	321	307	306	309	312	412	428	437	412		
12						311	304	308	308	308	307	306	309	312	355	410	426	430		
13						320	313	314	317	328	320	313	317	317	267	299	315	319		
14						316	313	315	313	317	316	313	315	317	297	290	281	279		
1 - REAR 1/2 BARREL FLANGE	314	313	314	317	328	307	306	309	312	321	309	306	309	312	263	294	306	312		
2						311	304	308	308	308	314	318	315	313	269	299	310	312		
3						309	309	312	314	326	302	296	301	299	304	281	294	297	279	
4						295	296	298	300	313	314	310	315	315	254	281	294	290		
5						312	310	314	316	328	314	310	315	315	265	297	310	315		
6						307	306	309	312	321	311	306	308	310	260	290	294	288		
7						302	303	307	309	321	304	301	306	304	258	292	294	285		
8						323	324	325	327	340	325	325	326	326	272	306	319	324		
9						330	332	332	337	347	334	329	336	336	279	312	330	332		
10						305	306	309	319		309	304	308	306	309	265	292	306	310	
11						307	308	309	314	324	311	318	313	313	269	297	312	315		
12						320	320	321	321	335	320	317	322	325	274	306	315	321		
13						237	230	232	229	227	232	230	230	233	219	219	222	220		
14						164	168	168	171	169	174	168	168	171	161	174	171	168		
10 MIX. AT INTAKE PORT						92	96	96	99	99	90	93	96	96	79	79	76	76		
" " BLOWER RIM						95	99	99	102	102	93	99	100	102	79	79	76	76		
FUEL - SUC. SIDE PUMP						90	93	93	93	96	91	93	93	96	82	79	72	72		
" " PR. " "						66	64	63	63	57	66	63	60	63	82	72	59	55		
" " CARB. FLOAT CHAMBER						84	84	84	81	81	87	84	81	84	99	92	82	79		
11 - FRT. SP. PL. ELBOW						50	50	47	42	39	51	45	42	44	70	54	38	60		
11 - REAR. " " "						51	51	48	42	39	54	48	40	45	72	55	38	65		
RECORDED FREE AIR						49	48	45	42	39	51	45	42	45	72	55	38	65		
AIR - CARB. SCOOP						57	60	57	57	57	60	60	57	57	76	59	45	59		
" " FRT. CYL. 14						148	151	154	157	163	154	151	163	157	165	174	174	178		
" " FRT. CYL. 1						84	84	84	81	81	89	84	84	87	89	79	69	86		
" " REAR. " "						148	146	148	145	148	154	147	146	146	148	148	139	135		
" " OIL COOLER EXIT						219	217	219	219	225	217	217	217	217	194	203	210	205		
OIL - IN LINE						119	119	119	119	122	122	119	119	119	122	139	139	132		
OIL - OUT						107	108	108	107	105	112	109	108	108	110	102	99	86		
ACCESSORY COMPT.						102	102	105	102	102	99	100	102	99	102	96	92	86		
LEFT MAGNETO						87	90	93	90	90	87	90	89	75	82	76	69	65		
PILOT'S COCKPIT																				
RECORDING INSTR. COMPT.																				

TABLE 2

TEMPERATURE DATA (SHEET 2)

(SHEET 2)

TEST NO-FLIGHT NO. RUN NO.	19-1					19-2					20-1					20-2				
	1	2	3	4	5	1	2	3	4	5	1	2	3	4	1	2	3	4		
TRUE AIRSPEED, MPH	332	331	332	330	330	331	331	331	332	334	154	153	153	151	138	135	136	136		
Qc, IN H ₂ O	35.0	33.7	32.8	31.4	30.3	34.0	33.0	31.7	30.8	33.9	11.7	11.5	11.5	11.2	9.4	9.0	9.1	9.1		
ATM. PRESS. IN. HG	17.48	16.83	16.16	15.51	14.90	16.89	16.22	15.59	14.94	16.53	4600	10800	14700	18800	4000	9900	14900	18600		
ATM. TEMP. °F	33	30	27	21	18	26	23	23	20	27	62	42	31	19	67	44	28	19		
ρ DENSITY RATIO	.616	.596	.576	.560	.541	.603	.583	.560	.540	.589	850	905	807	720	939	900	758	650		
DENSITY ALT., FT	15650	16700	17700	18500	19600	16500	17300	18500	19650	17050										
B.H.P.	928	900	877	849	816	909	877	853	812	905										
R.P.M.						2680														
MAN. PRESS IN. HG						40.5	39.0	37.6	36.3	34.9	39.2	38.0	36.5	35.0	38.6					
						HIGH SPEED					HIGH SPEED									
CYL NO	PT OF MEASUREMENT	TEMP. °F																		
1	- REAR SP. PL. GASKET	377	375	378	382	388	389	383	397	393	379	387	403	401	401	376	381	352	331	
2		375	375	379	382	388	383	389	399	395	381	387	403	398	394	381	381	352	329	
3		384	379	384	388	393	392	395	409	406	388	392	410	401	403	390	386	358	336	
4																				
5																				
6																				
7																				
8																				
9																				
10																				
11																				
12																				
13																				
14																				
1	- REAR & BARREL FLANGE	307	302	304	304	311	305	313	318	318	300	298	311	311	311	283	297	290	278	
2		309	300	307	309		302	304	311	309	295	288	305	305	305	283	299	285	280	
3		302	295	298	298	302	302	304	313	313	295	298	311	311	309	283	292	285	278	
4																				
5																				
6																				
7																				
8																				
9																				
10																				
11																				
12																				
13																				
14																				
10	MIX. AT INTAKE PORT	304	300	302	302	304	304	304	313	313	297	288	300	302	302	278	290	285	276	
"	BLOWER RIM	313	309	311	313	316	316	316	316	322	322	309	300	313	316	316	288	299	290	283
"	SUC. SIDE PUMP	221	219	219	219	219	219	222	225	223	223	229	220	215	211	225	211	204	194	
"	PR.	169	163	160	160	160	167	164	164	167	162	177	179	174	165	166	181	169	155	
"	CARB. FLOAT CHAMBER	89	92	92	92	92	88	91	96	93	93	82	79	79	76	84	84	84	81	
11	- FRT SP. PL. ELBOW	92	94	94	94	94	93	93	96	96	99	82	82	79	76	87	84	84	81	
12	- REAR	89	89	89	89	89	88	88	91	93	91	82	79	76	73	87	81	78	75	
13	"	68	65	62	59	59	64	62	64	62	64	85	68	62	50	84	78	46		
14	"	77	74	73	71	68	73	70	73	70	76	102	88	79	68	107	90	75	64	
RECORDED FREE AIR	48	46	42	39	36	44	41	41	38	44	66	48	38	22	70	50	36	25		
AIR - CARB. SCOOP	51	48	45	42	39	47	41	44	41	47	68	50	36	24	73	55	37	19		
" - FRT. CYL. 14	51	45	42	42	36	44	41	41	38	44	68	50	36	24	73	55	37	19		
" - FRT CYL 1.	54	51	51	45	42	50	47	47	44	50	76	56	47	33	78	60	46	37		
" - REAR - "	143	141	146	149	154	139	142	148	148	139	177	179	179	177	183	144	133			
" - OIL COOLER EXIT	83	80	80	77	74	82	79	79	79	79	93	82	76	65	93	87	75	60		
OIL - IN LINE	146	141	138	138	138	142	139	142	148	139	144	138	135	132	147	141	135	133		
OIL - OUT	219	214	214	214	214	217	212	217	217	209	204	215	215	209	197	205	202	197		
ACCESSORY COMPT.	116	115	115	112	112	114	114	116	114	114	107	96	90	82	107	98	87	78		
LEFT MAGNETO	106	106	103	103	103	105	102	105	102	99	96	93	90	85	98	95	90	84		
PILOT'S COCKPIT	94	94	94	92	92	93	93	93	93	93	85	79	76	70	93	84	78	69		
RECORDING INSTR. COMPT.	74	73	71	68	68	82	85	85	88	85	90	82	76	70	95	87	78	69		

TABLE 2

TEMPERATURE DATA (SHEET 3)

TEST NO.-FLIGHT NO. RUN NO.	22-1					22-2					IND. AIRSPEED Q.C. IN. H ₂ O ATM. PRESS., IN. HG. ATM. TEMP., °F DENSITY RATIO DENSITY ALT., FT. B. H. P. R. P. M. MANIF. PRESS, IN. HG.	21-1A				21-1B			
	1	2	3	4	5	1	2	3	4	5		1	2	3	4	1	2	3	4
TRUE AIRSPEED M. P. H.	331	331	331	330	330	329	329	330	330	327	IND. AIRSPEED Q.C.	155	153	152	152	140	137	135	135
ATM. PRESS., IN. HG.	346	337	323	310	303	33.9	32.8	31.9	30.8	29.2	AV. PRESS. ALT.	11.8	11.4	11.3	11.3	9.6	9.2	9.0	8.9
ATM. TEMP., °F	17.23	16.54	15.90	15.27	14.66	17.16	16.47	15.84	15.19	14.60	AV. FREE AIR, °F	4600	9400	14200	17600	5200	8100	14300	17700
DENSITY RATIO	.28	.23	.23	.19	.13	.28	.26	.23	.21	.19	AV. B. H. P.	52	47	37	24	55	53	35	19
DENSITY ALT., FT.	.616	.594	.571	.553	.538	.610	.588	.569	.548	.529	AV. MANIF. PRESS.	941	930	845	762	1019	933	771	680
B. H. P.	15650	16750	17950	18900	19700	15950	17050	18050	19150	20200	R. P. M.	39.8	39.9	36.1	31.9	42.9	43.1	35.5	30.8
R. P. M.	928	900	877	840	816	919	891	863	830	793	2560	2560	2560	2560	2540	2540	2540	2540	
MANIF. PRESS, IN. HG.						39.9	38.2	36.8	35.3	34.2	AUTO RICH CLIMB NO SPINNER					FULL RICH CLIMB OR CUFFS			
CYL. NO.-PT. OF MEASUREMT	TEMP, °F					HIGH SPEED													
1 - REAR SP. PL. GASKET	369	367	372	374	379	377	368	373	377	377		383	406	406	406	361	390	352	338
2	369	365	372	374	379	373	366	370	373	375		381	401	397	394	359	385	350	332
3	374	366	374	379	383	377	370	375	379	382		390	403	394	397	366	390	356	341
4												390	399	390	390	361	383	350	332
5																			
6																			
7																			
8																			
9																			
10																			
11																			
12																			
13																			
14																			
1 - REAR & BARREL FLANGE	313	327	306	306	306	312	303	303	305	305		296	309	312	325	294	303	294	282
2																			
3																			
4																			
5																			
6																			
7																			
8																			
9																			
10																			
11																			
12																			
13																			
14																			
10-MIX. AT INTAKE PORT	302	293	293	297	299	301	294	294	296	298		289	303	305	305	289	298	289	280
" " BLOWER RIM	304	299	299	302	304	303	301	301	303	303		294	309	309	307	296	305	291	282
FUEL - SUCTION SIDE PUMP	291	286	286	288	288	291	287	287	290	290		280	294	294	294	280	287	278	271
" " PRESS.	304	302	302	304	303	301	301	303	303	305		291	307	309	309	294	303	298	289
" " CARB. FLOAT CHAMBER	302	295	297	297	297	301	296	296	298	298		287	298	303	300	282	291	284	278
11 - FRT. SP. PL. ELBOW	293	288	291	291	288	294	290	291	291	291		284	298	303	303	284	294	289	282
" " REAR " " "	320	313	315	315	318	319	314	314	316	316		303	318	325	323	303	309	309	303
RECORDED FREE AIR	327	325	325	327	327	327	325	325	325	327		307	330	336	332	314	327	323	314
AIR CARB SCOOP	302	297	297	297	299	301	298	298	301	301		289	303	309	305	291	296	291	282
" FRT. CYL. NO. 14.	81	86	86	89	89	91	93	91	93	96		300	318	323	321	303	309	298	289
" FRT. CYL. NO. 1	81	81	81	81	81	85	88	82	88	88									
" REAR " " "	75	69	69	66	64	73	76	68	68	68		223	221	221	213	221	213	204	195
OIL - IN LINE	219	215	215	215	218	218	216	216	216	216		166	174	172	169	169	174	166	158
" OUT	145	140	140	137	137	150	144	142	142	142		77	77	77	77	77	77	77	74
ACCESSORY COMP'T.	220	214	212	212	212	221	216	208	213	216		80	80	77	77	77	77	77	74
LEFT MAGNETO	115	109	109	109	106	113	113	111	111	111		80	74	74	74	74	74	74	72
PILOT'S COCKPIT	101	101	95	98	95	105	105	96	99	99		91	91	91	88	94	97	97	91
RECORDING INSTR. COMP'T.	89	89	86	86	84	85	91	88	85	85		80	77	71	68	74	77	72	51
	81	81	81	81	78	71	71	68	68	64		80	77	74	68	77	80	80	54

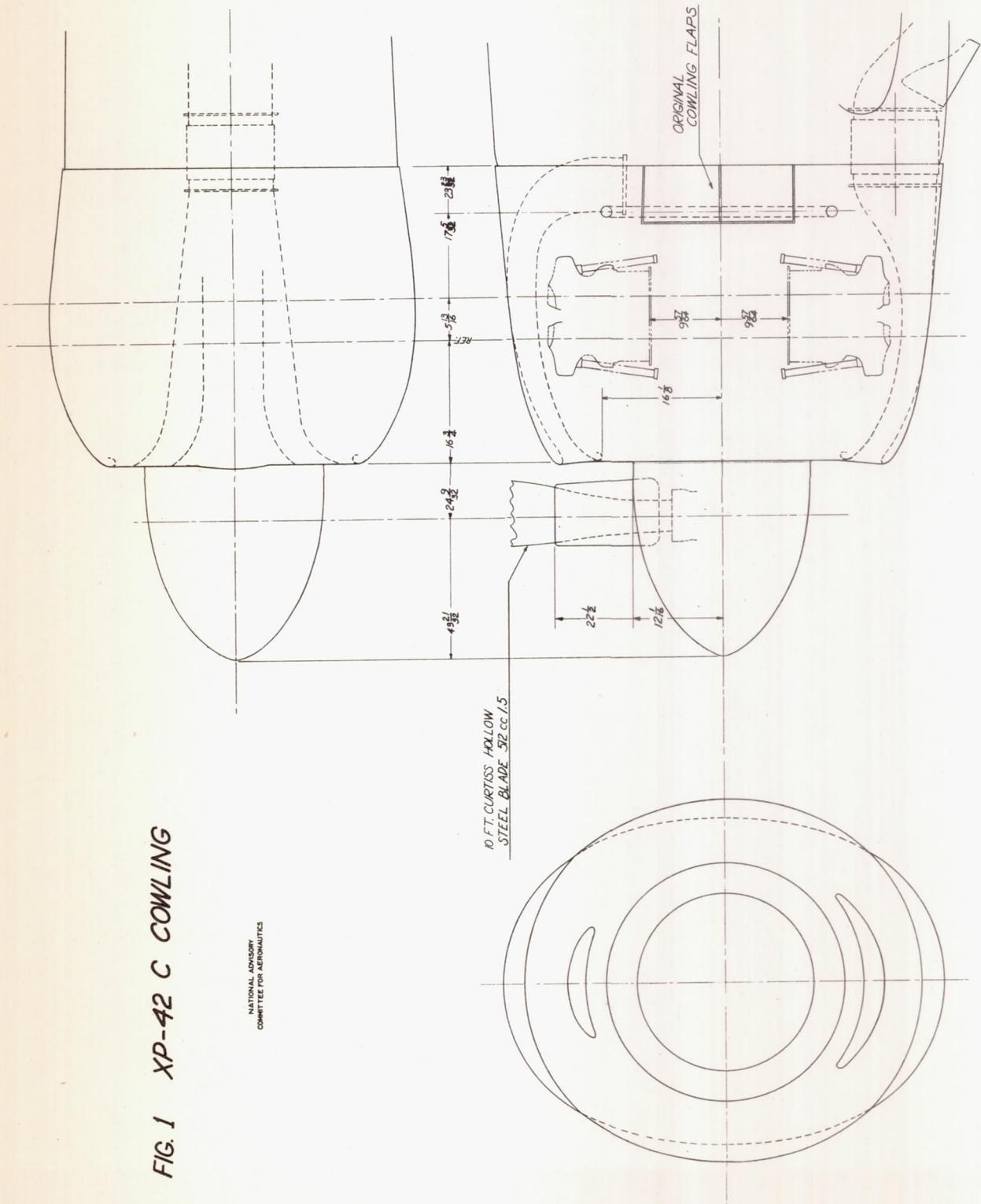
Table 3: Speed and Pressure Recovery Data from Flight Investigations of XP-42 Airplane.

Long Nose	S.N.-H.I.V.			S.N.-L.I.V.					C-Cowl		
	with cuffs	Cuffs	No cuffs	Fan and #1 Cuffs	Fan Only	#1 Cuffs	#2 Cuffs	No Cuffs	Spinner Cuffs	Cuffs Only	No Cuffs or Spinner
①	344	339	340	337	339	339	342	343	339	337	336
②	.83	.80	.74	.87	.84	.80	.77	.76	.69	.74	.74
③	.86	.70	.62	1.02	.98	.86	.84	.74	.58	.68	.67
④	.83	.70	.62	.95	.95	.81	.82	.75	.58	.69	.68

- ① Maximum Speed at 1000 hp. at 14500 ft.-mph true airspeed
- ② Pressure recovery on front of engine at high speed, P/q_c
- ③ Pressure recovery in 140-mph, (indicated airspeed) climb
- ④ Pressure recovery in 155-mph climb (indicated airspeed)

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FIG. 1 XP-42 C COWLING

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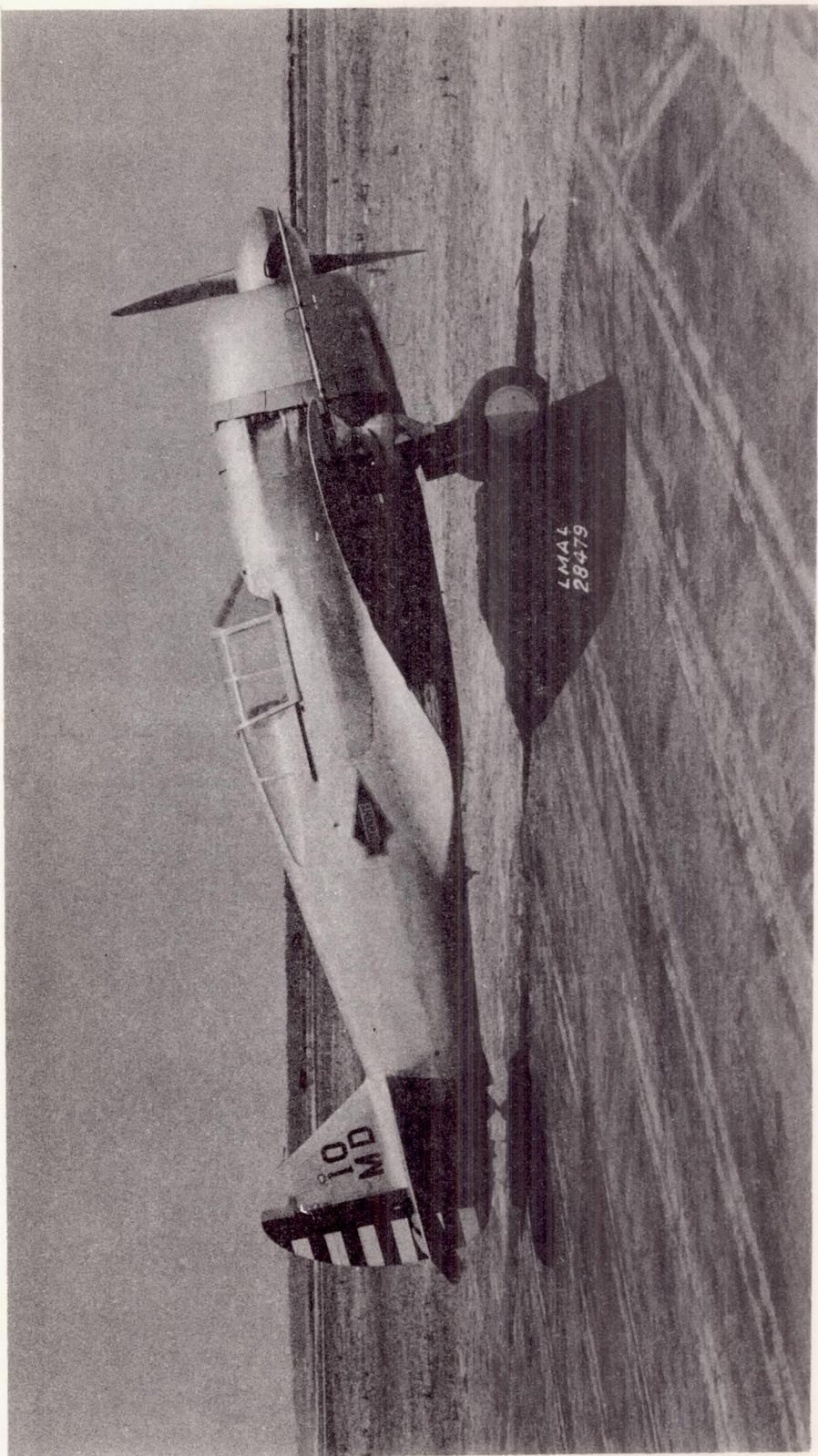


Figure 2. - Side view of airplane with C cowl, spinner, and cuffs.

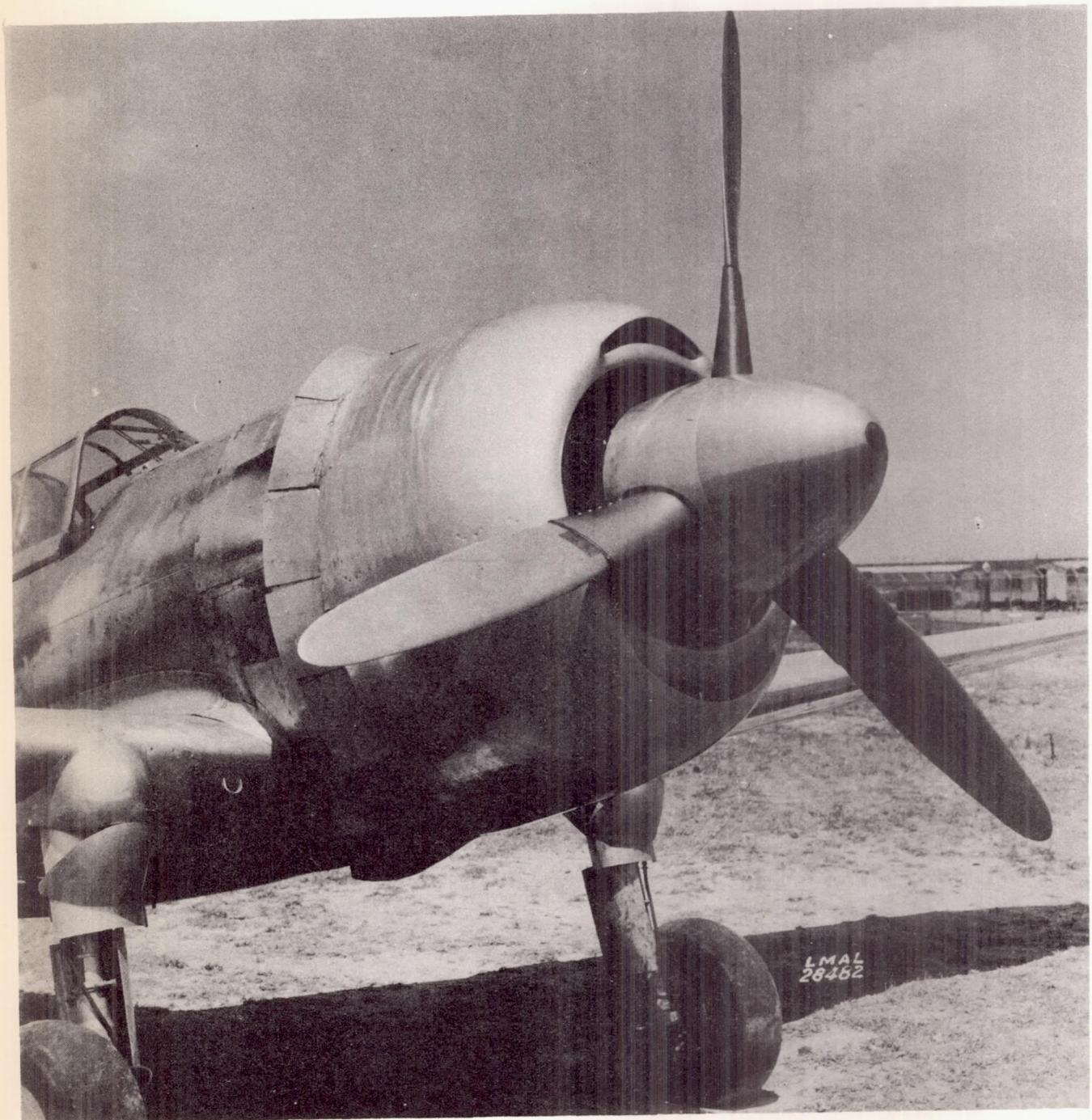


Figure 3.- Close-up of cowling with spinner and cuffs.

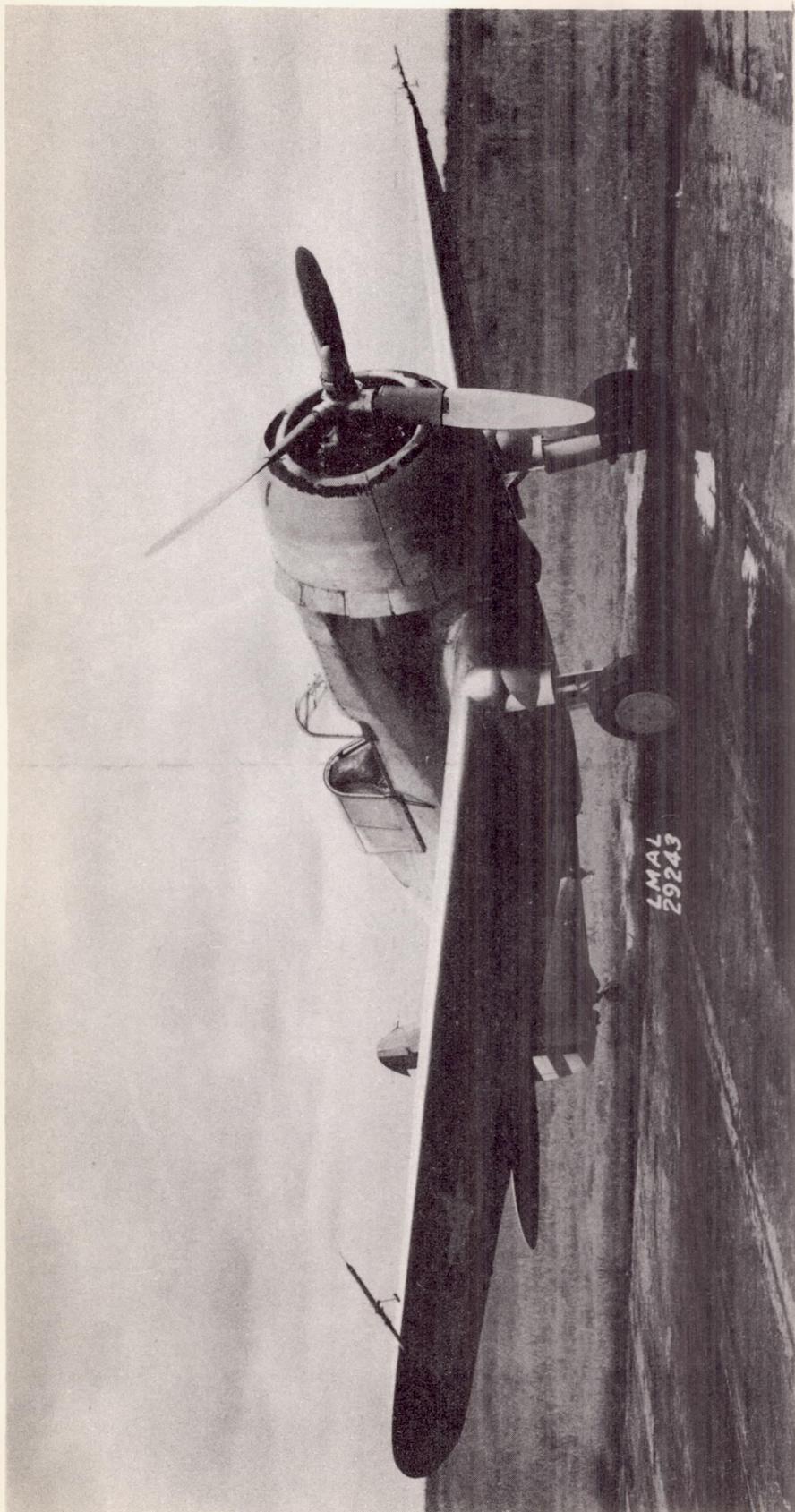


Figure 4.- Three-quarter front view of airplane with C cowl, cuffs only.

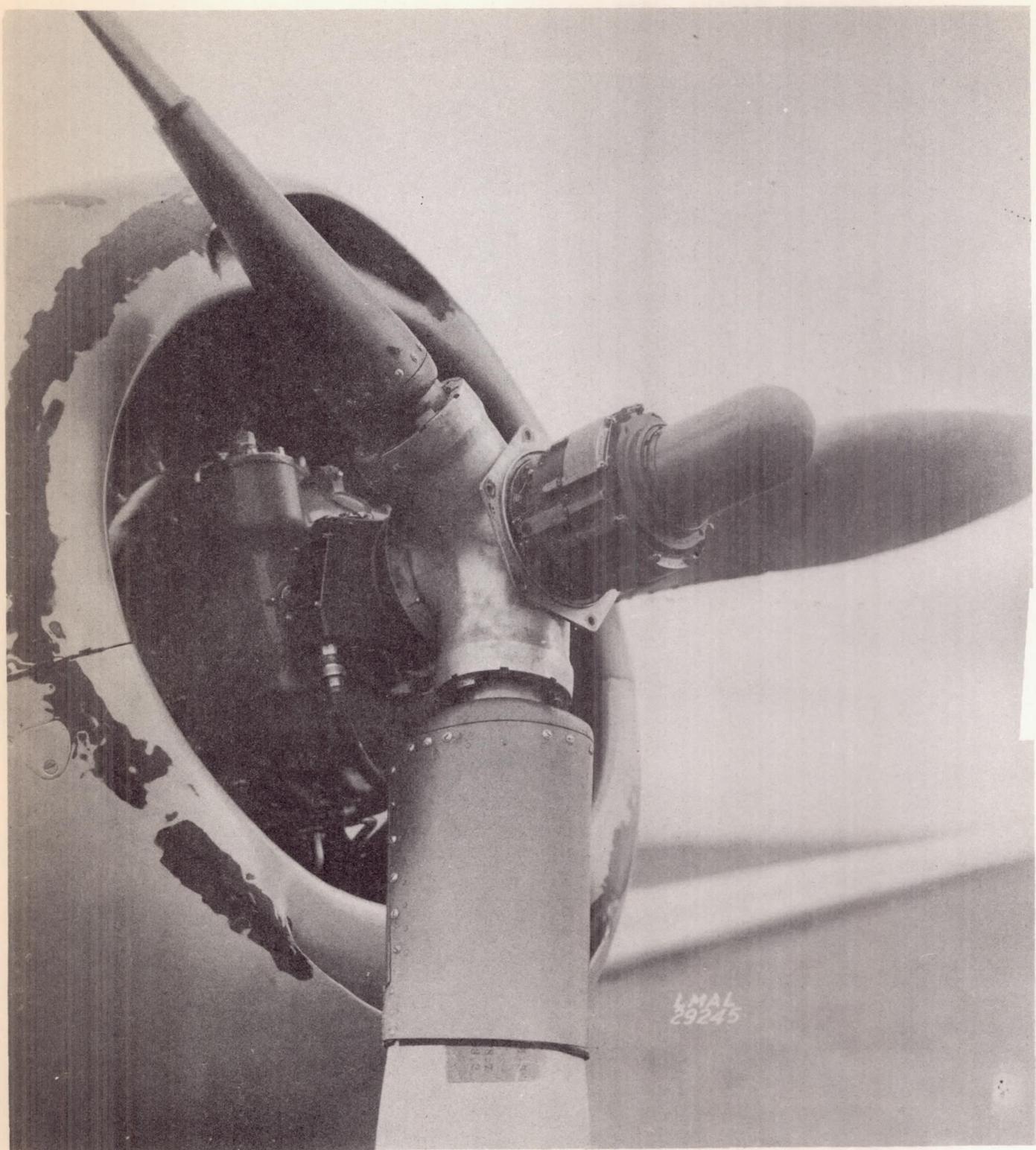


Figure 5.- Close-up of cowling with cuffs only.

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Figure 6.- Front view of cowling without spinner or cuffs.



Figure 7.- Close-up of cowling without spinner or cuffs.

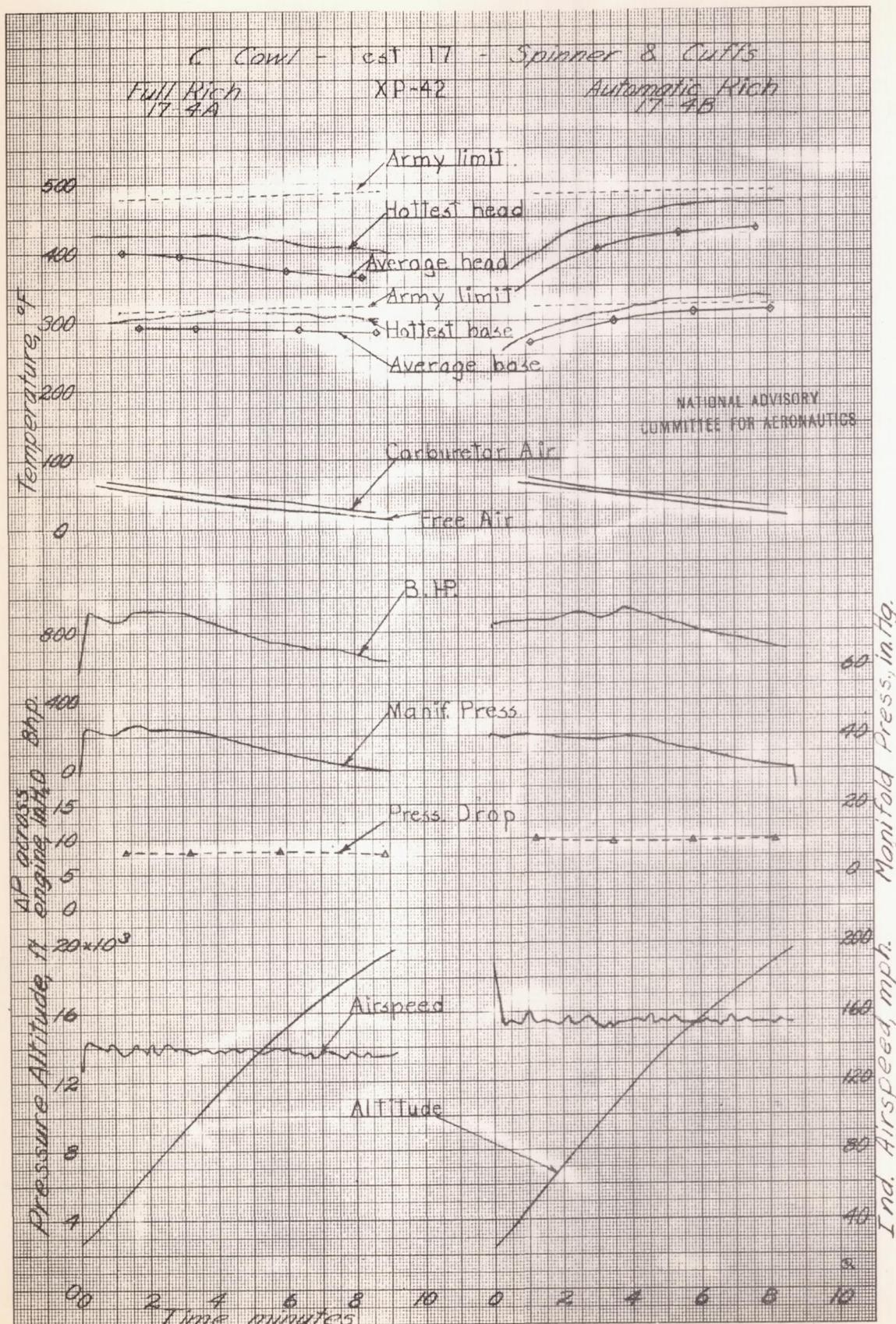
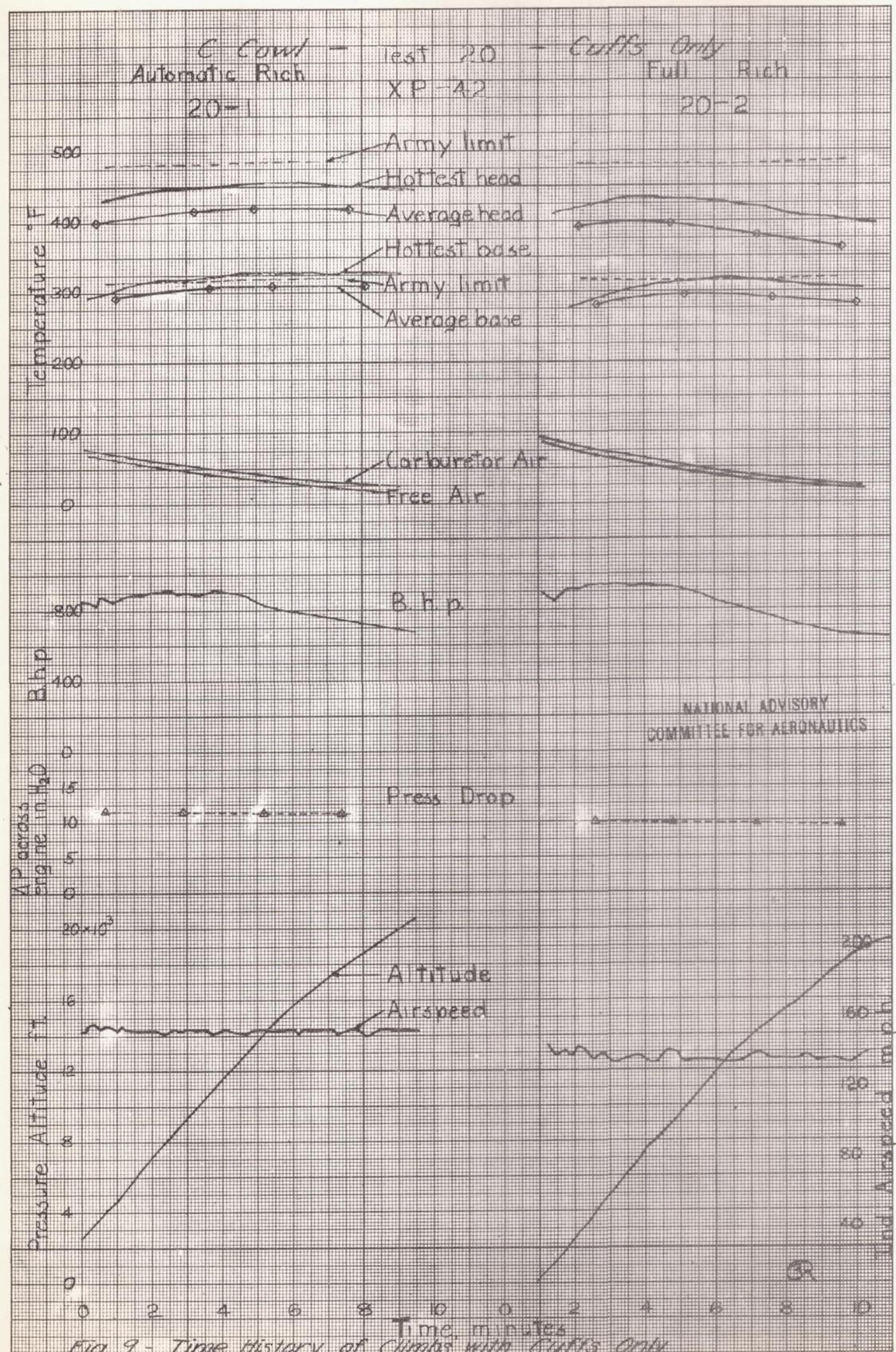


Fig. 8 Time History of Climbs with Spinner & Cuffs



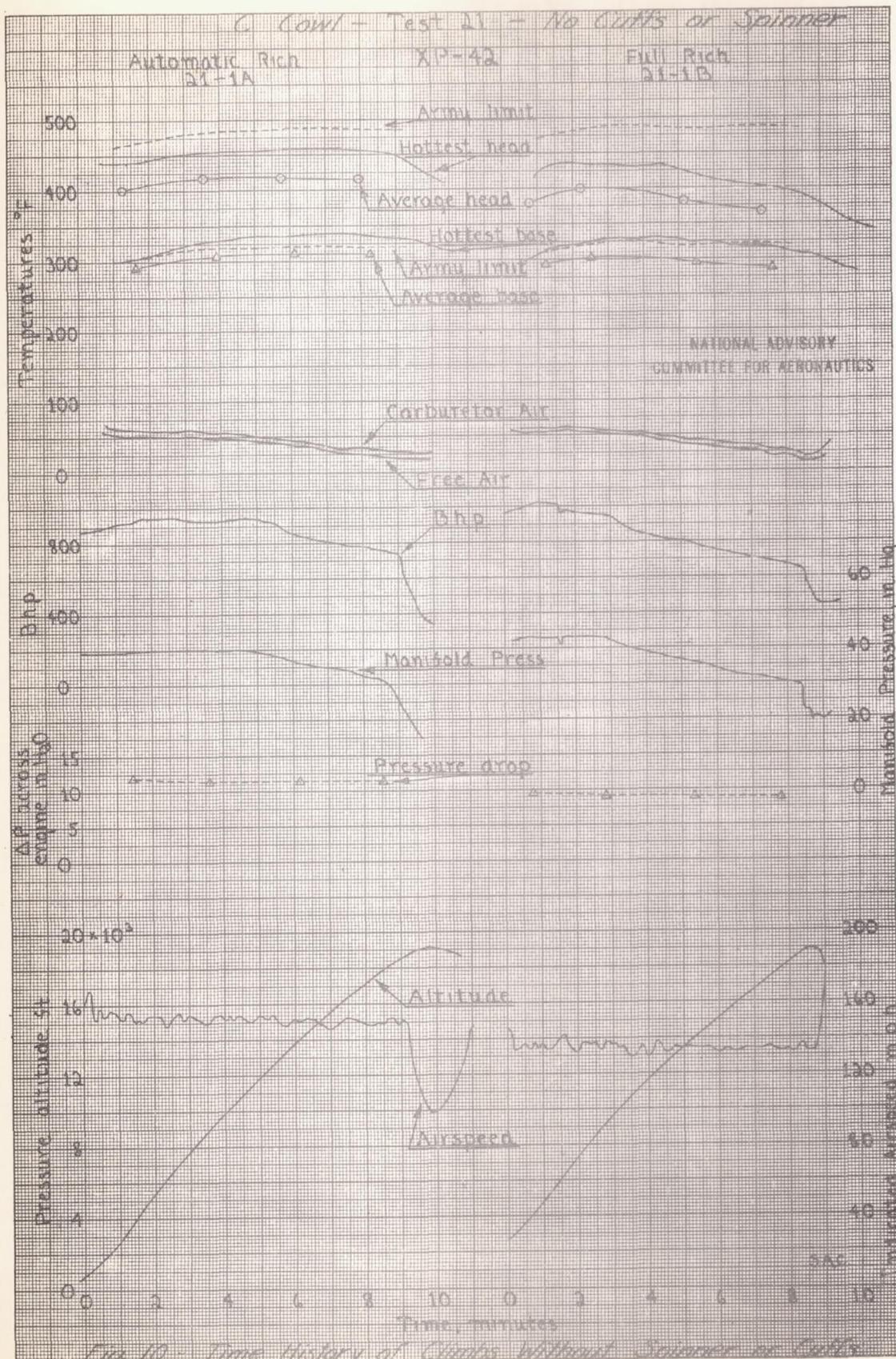
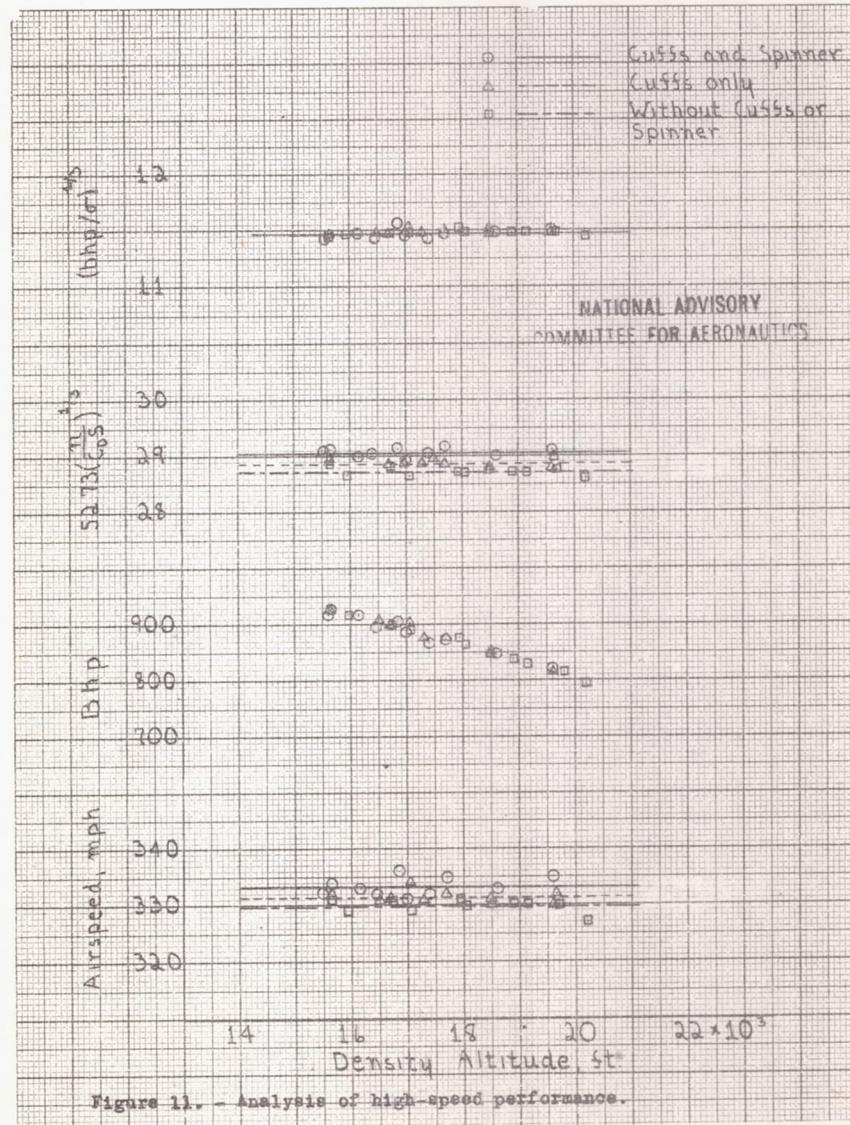


Fig. 10. Time history of counts without spores at 1000



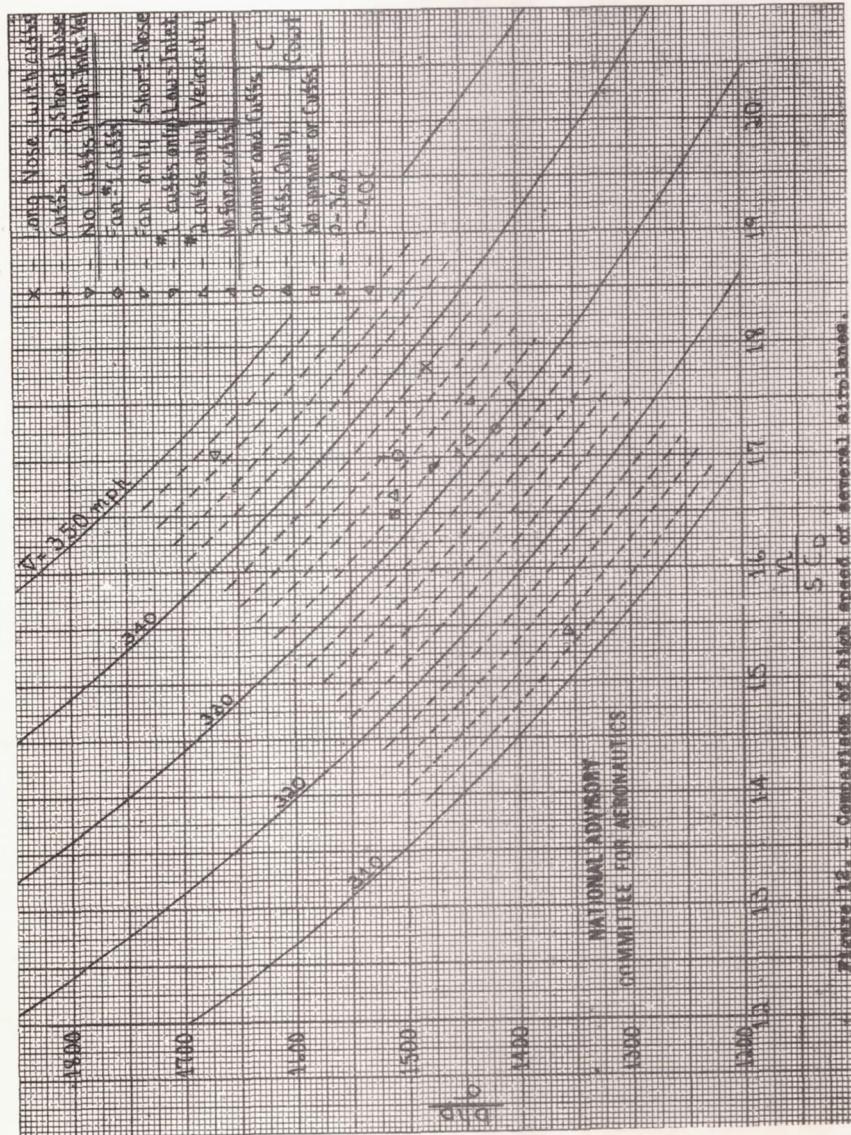


Figure 12 - Comparison of high speed or several airplanes.

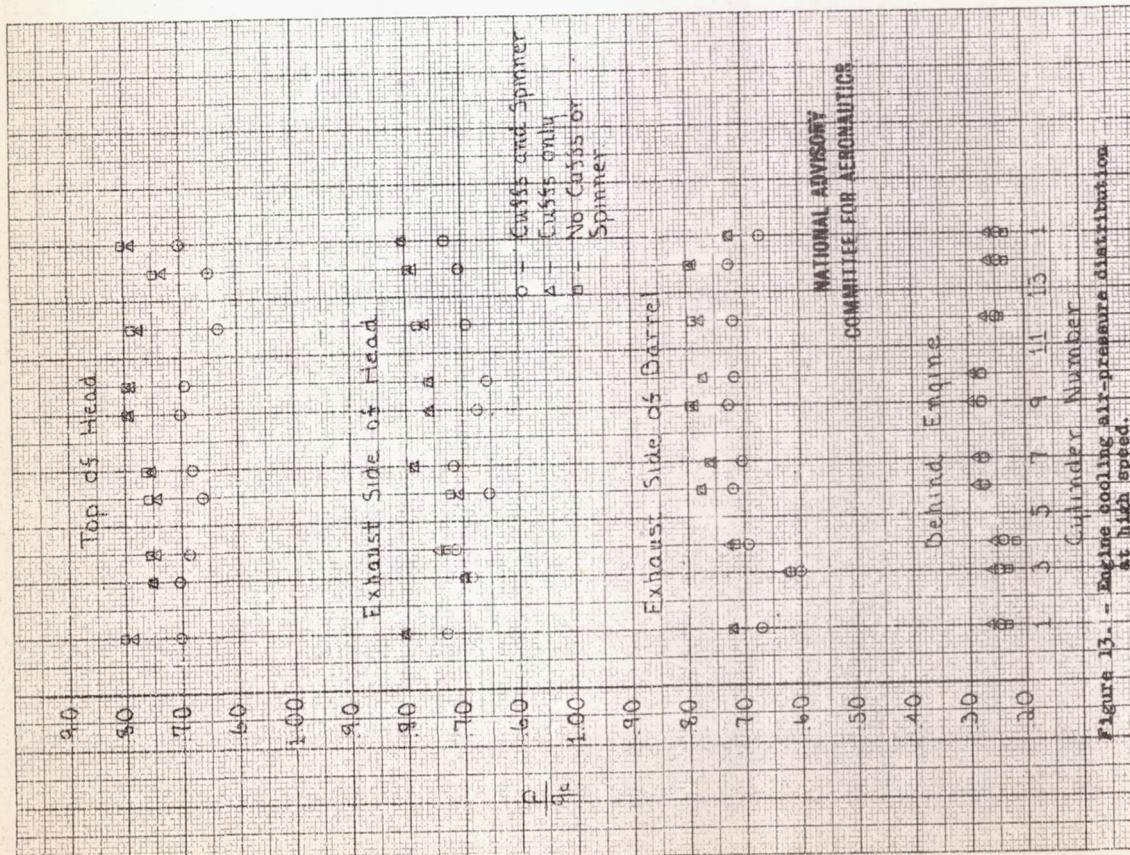


Figure 13. — Engine cooling air-pressure distribution at high speed.

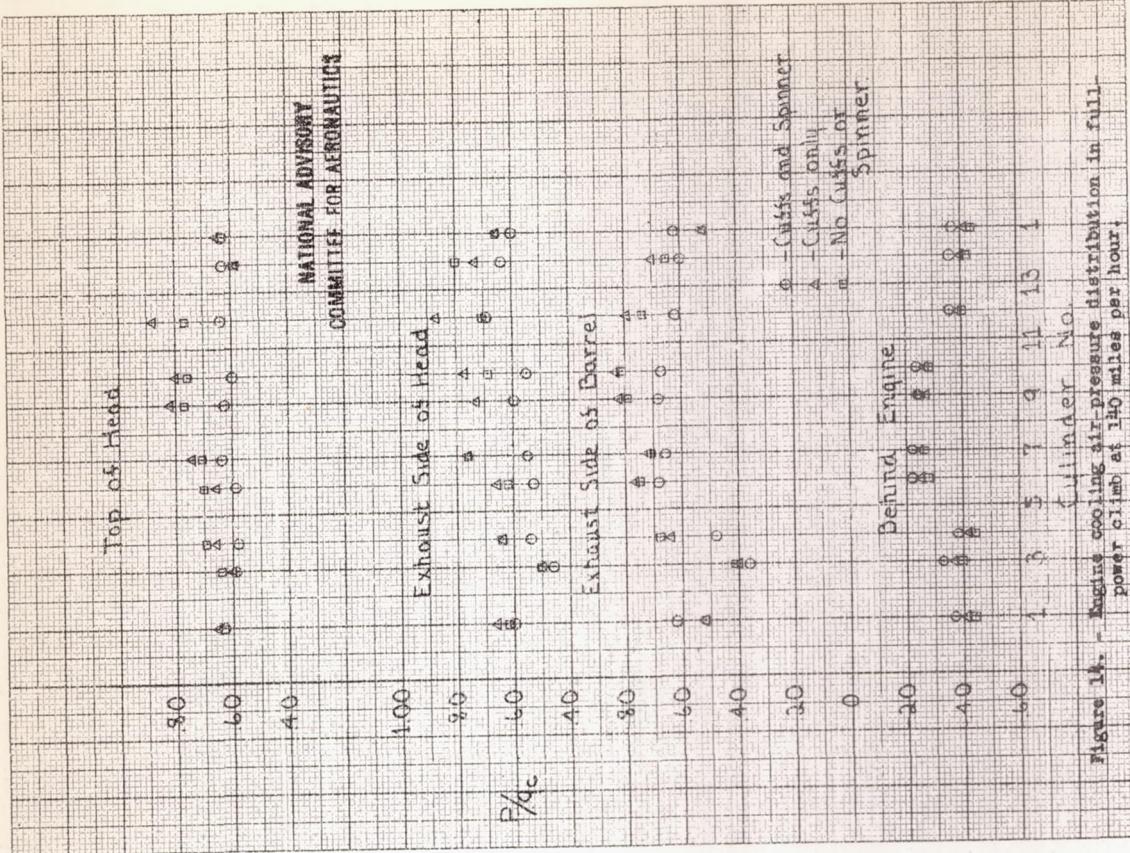
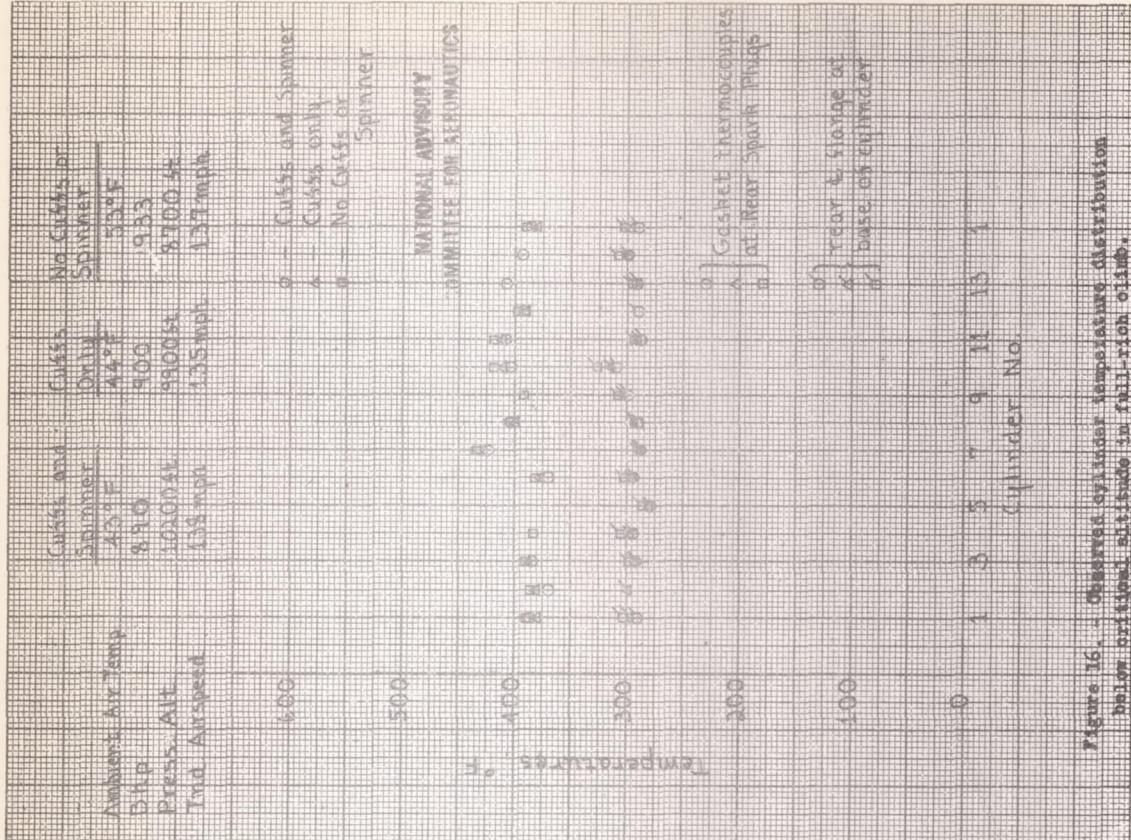
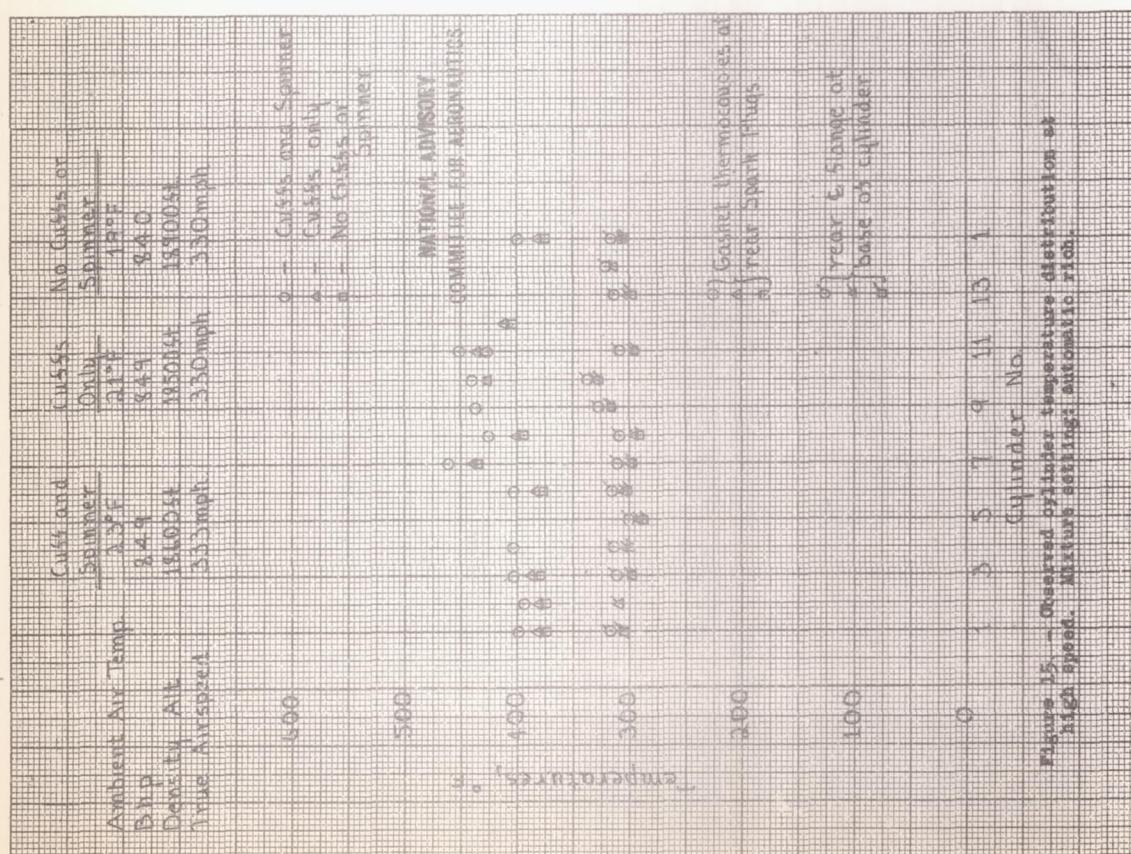


Figure 14. - Engine cooling air-pressure distribution in full power climb at $\frac{1}{3}$ miles per hour.



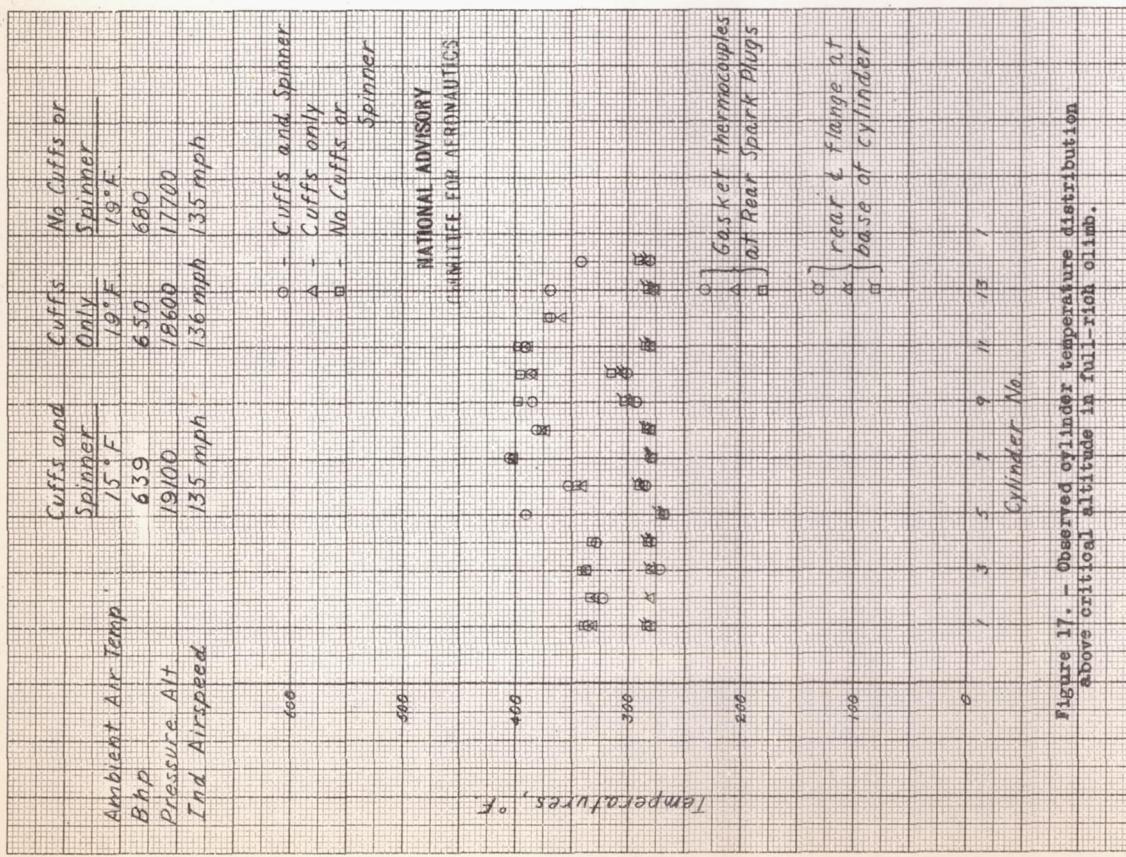


Figure 17. - Observed cylinder temperature distribution above critical altitude in full-rich climb.

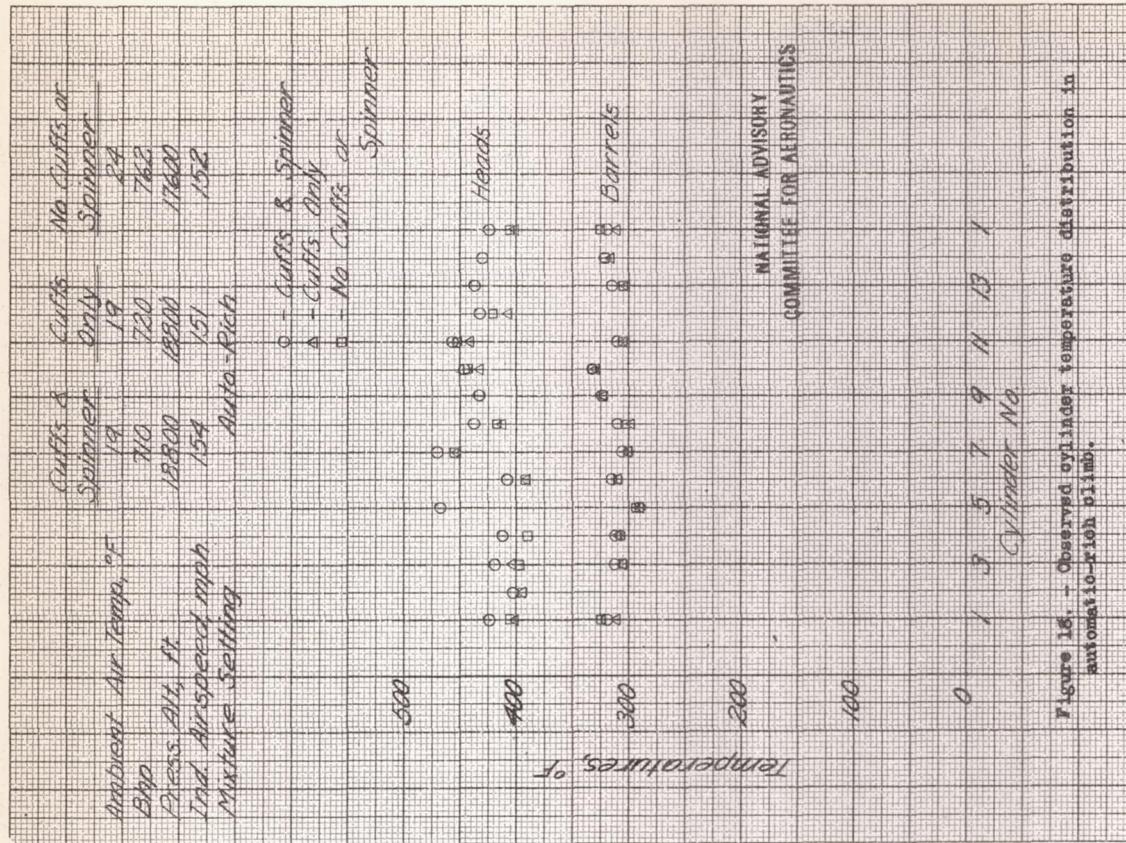


Figure 18. - Observed cylinder temperature distribution in automatic-rich climb.

